

This HANDBOOK of data on all RCA tubes has been compiled to meet the requirements of electronic engineers for tube information which can be kept up-to-date. Its convenient, loose-leaf form permits the revision of data on existing tubes and the addition of data on new tubes as they are made available.

The material is arranged in sections with tabbed separators to facilitate quick reference. The general section contains a table of contents for the complete Handbook, a detailed explanation of tube ratings and typical operating conditions, tube outline drawings, base drawings, and other useful information concerning tubes. The other sections, indexed according to tube classes, contain ratings, characteristics, operating conditions, and curves for the many different tubes in those classes.

The RCA Tube Handbook is especially useful to designers of tube equipment but will prove helpful to anyone having need for concise data on our various tubes. If further data on any tube type are desired, we shall be glad to be of assistance.

TUBE DEPARTMENT
RADIO CORPORATION OF AMERICA, HARRISON, NEW JERSEY

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Commercial Engineering
TUBE DEPARTMENT
RADIO CORPORATION OF AMERICA, HARRISON, NEW JERSEY

### RCA TUBE HANDBOOK HB-3

# GENERAL SECTION



The information in this section, in general, applies to all classes of RCA tubes. It includes the Index of Contents for all sections, preferred-type lists, discussion of ratings, drawings of bases, caps, and tubes, as well as other general information of interest to the equipment designer.

For further Technical Information, write to Commercial Engineering, Tube Department, Radio Corperation of America, Harrison, N. J.



Tube types are listed below in numerical-alphabetical-numerical sequence. For each type, on X-mark (or a "-mark) in one of the eight columns headed SECTION indicates the particular section in which that type will be found. The X-marks in the column for any section give the arrangement of the general material and the tube types in that section. The sections are keyed as follows:

Reference is to front of sheet only unless otherwise indicated

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6BJ6			İ		ĺ	×			6-20-47	6BJ6 Tent. Data
	ļ					X				Curve 92CM-6867
	1					Х				Curve 92CM-6870
6BL7-GT		ì	l	ŀ		Х			10-1-53	6BL7-GT Data
6BQ6-GT		i				X			5-1-52	6BQ6-GT Data
						Х			ŀ	Curve 92CM-7459
6BQ7						X			5-1-51	6BQ7 Tent. Data
						X			5-1-51	Circuits CE-7643-7644
						X				Curve 92CM-7538
	1			1		X	1			Curve 92CM-7550
6BQ7-A	ı			1		×	1		11-1-52	6BQ7-A Tent, Data
	1			1		×	1		11-1-52	Circuits CE-7643-7644
	1			1		×	1		l	Curve 92CM-7538R1
	1			1	1	X	1		l	Curve 92CM-7550R1
6C4	1			1		X			6-1-42	6C4 Tent. Data
	1	1		l	ĺ	X	1		l	Curve 92C-6378
6C5, 6C5-GT	1				1	X	i		3-20-43	6C5, 6C5-GT/G Data
	1			l	1	X		1		Curve 92C-4511
6C6	1					X	1		6-15-48	6C6 Data
6C8-G		1				×			12-1-41	6C8-G Data
6CB6		1				X		1	2-1-50	6CB6 Tent. Data
						×	ľ	l	l	Curve 92CM-7375
6CD6-G	1	1	1		1	X	l	l	2-1-50	6CD6-G Tent. Data
	1		1			X			2-1-50	Circuit CE-7405R1
	4		1		1	l x		,		Curve 92CM-7393



	- 11	NDE	<b>X</b> -			-	_	_	١	
	_								CONT	TENTS
Tube Type	G	c	P	Sec	H	R	s	т	Date	Sheet
6CF6						x	Т		8-1-53	6CF6 Tent. Data
6CL6	li	i				х			9-1-52	6CL6 Tent, Data
						X			9-1-52	Circuit CE-7804
	i					Х	١.			Curve 92CM-7802
	П		1			Х				Curve 92CM-7808
6D6						X			9-2-41	6D6 Data
6D8-G		Ì	ı			X			2-2-40	6D8-G Data
6E5			l	1		×			12-15-44	
6F4	1		l		X				8-15-44	6F4 Tent. Data
					×					Curve 92CM-6567 .
6F5, 6F5-GT				]		X		1	6-20-47	6F5, 6F5-GT Data
6F6, 6F6-G						X			5-1-42	6F6, 6F6-G Data
			1			X			5-1-42	Data 2
						X			1	Curve 92C-4440
6F7						X			9-1-35	6F7 Data
						X			1, , , , ,	Curve 92S-5426
6F8-G						X			1-1-43	6F8-G Data See 6US/6G5
6G5						x			4-1-44	6G6-G Data
6G6-G						×			7-1-74	Curve 92CM-6122R1
CUE CHE CT	Н					X			8-1-42	6H6, 6H6-GT/G Data
6H6, 6H6-GT					v	^			4-1-44	6J4 Tent. Data
6J4					X				~-,	Curve 92CM-6543
6J5, 6J5-GT	l				^	×			9-1-50	6J5, 6J5-GT Data
וט-נוס ,ניט	l I					î				Curve 92CM-6448
616						â			10-1-51	6J6 Data
616						â				Curve 92CM-6403R1
						â			ļ ,	Curve 92CM-7672
6J7, 6J7-G,						^				24.70 /24 7012
6J7-GT						×			6-15-48	6J7, 6J7-G, 6J7-GT Data 1
J G						x			6-15-48	Data 2
						x			" "	Curves 92CM-6007R1
6J8-G		1				x			7-1-41	6J8-G Tent. Data
6K5-GT						x			1-1-43	6K5-GT/G Data
6K6-GT						x			10-1-51	6K6-GT Data 1
						x			10-1-51	Data 2
	l					×				Curve 92CM-4881R2
						×				Curve 92CM-6313
6K7, 6K7-G,										
6K7-GT		ļ				×			9-2-41	6K7, 6K7-G, 6K7-GT Data
6K8, 6K8-G,		ı								
6K8-GT		ı				×			5-1-41	6K8, 6K8-G, 6K8-GT Data
6L4		ı			X				5-20-49	6L4 Tent, Data
					X					Curve 92CM-7202
6L5-G						×			4-20-38	6L5-G Data
6L6, 6L6-G						X			5-1-42	6L6, 6L6-G Data
						X			5-1-42	Data 2
						X				Curve 92C-4581R1
						X			ا م م م ا	Curve 92C-4608
6L7, 6L7-G						Ŋ			2-2-40	6L7, 6L7-G Data
					-	×××	-			Curve 92C-4447
	ı	- 1			- 1	Ŋ	ŀ		1 }	Curve 92C-4531 Curve 92C-4536
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Tube Type	Ļ	c	P	Sec	M	R	s	T	Dete	Sheet
	9	۲	Ļ	-	_	<u>`</u>	•	•		
6N5										See 6AB5/6N5
5N6-G	ŀ	1	1			X			12-1-39	6N6-G Tent. Data
6N7, 6N7-GT		1	i			X			6-1-42	6N7, 6N7-GT/G Data
	1		ı			X				Curve 92C-4611
6P5-GT		t		1		"			12-1-42	6P5-GT/G Data (on back of 6N7 curve 92C-46
		ľ								CHIAN 23C-40
6Q7, 6Q7-G,						l.			12-1-41	6Q7, 6Q7-G, 6Q7-GT Data
6Q7-GT		l				×		ļ	12-1-41	Curve 92C-4522R2
						â			12-1-43	6R7, 6R7-GT/G Data
6R7, 6R7-GT		1	ļ	ļ		x			2-1-50	6S4 Tent. Data
6 <b>S4</b>					'	â			2-1-50	Curve 92CM-7373
				1	1 1	â			2-2-40	6S7, 6S7-G Data
6\$7, 6\$7-G						ŝ	1	1		6S8-GT Tent. Data
6S8-GT	l	1				ŝ			8-29-47	Curve 92CM-6876
-C 1 7			1			^	١.			Curve 92CIN-0070
6SA7,	1					×			1-1-43	6SA7, 6SA7-GT/G Data
6SA7-GT			l			Î			1-1-73	Curve 92C-4993
			ļ			Î				Curve 92C-4989
CCD7 1/		ł				۱ŵ	ļ		4-1-46	6SB7-Y Tent. Data 1
6SB7-Y						I â			4-1-46	Tent. Data 2
	1	1		ĺ	l	Î			4-1-40	Curve 92CM-6635
6SC7		i			1	١ŵ			3-15-41	6SC7 Data
6SF5, 6SF5-GT .		ļ	1		l	Ιŵ			5-1-41	6SF5, 6SF5-GT Data
6SF7		į .			ĺ	x			12-1-41	6SF7 Tent. Data
O3F1				1		Ιŵ			12-1-11	Curve 92C-6256
ccc3		ı	1		ļ	Ιŝ	1		5-1-42	6SG7 Tent. Data
6SG7				1	l	Ιŵ			)=1=12	Curve 92C-6248R2
6SH7		ł		1	İ	Ιŵ			6-1-42	6SH7 Tent. Data
03/17	1	ŀ		1	1	Ιŝ			• • • •	Curve 92C-6395
6SJ7, 6SJ7-GT .		l			ŀ	ĺχ			6-15-48	
0337, 0337-07.		1	[	1		ĺχ				Curve 92CM-4939R1
	1		i		1	ĺχ				Curve 92CM-6444R1
	1			1		x	1		i	Curve 92CM-6409R1
6SK7,	1	1			ŀ					_
6SK7-GT		1	i	1	1	x	l	١.	12-1-42	65K7, 6SK7-GT/G Data
05.17		ı	ŀ	ı	1	ĺχ		1		Curve 92C-4938
6SL7-GT		1				lх			7-1-41	6SL7-GT Tent. Data
6SN7-GT		ı		ļ	1	Ιx			4-1-44	6SN7-GT Data
6SQ7,	1	1	l		ŀ	l	ŀ	i		
6SQ7-GT				1	į.	l x	-		12-1-43	
•		1	ĺ	1	ı	Ι×		1		Curve 92C-6310
6SR7		ı	l	1	1	l x			4-15-40	6SR7 Tent. Data
6SS7		1		1	ı	ĺχ			5-1-41	6SS7 Tent. Data
6ST7	1	1	1	1	ı	١x			12-1-41	6ST7 Tent. Data
6SZ7	1	1	1	1	1	×		1	4-1-46	6\$Z7 Tent. Data
6T7-G		1	1	1	1	×			12-1-41	6T7-G Data
6T8		1	1	1	1	×			2-1-49	6T8 Data
		1	1	1		×				Curve 92CM-7063
6U5		1		1	1	×	1		9-2-41	6U5/6G5 Data
6U7-G		1		1	1	l x			9-2-41	6U7-G Data
		1	1	1	1	X	1		Į.	Curve 92C-6121



Tube Type			_	Sec	.,				CONT	ENIS
	L	ı		Sad						
6Ų8	G	C	P	F			S	Т	Date	Sheet
•••	Г		1	Т	Н	×	Г	_	4-1-53	6U8 Tent. Data
			l	l		X				Curve 92CM-7873
	1			l		х	ĺ			Curve 92CM-7871
6V6, 6V6-GT	L		ı	l		х			1-1-53	6V6, 6V6-GT Data
			ŀ	ŀ		х				Curve 92CM-4807R2
						Х				Curve 92CM-6339R1
6W4-GT	1					Х			3-1-51	6W4-GT Data
						×				Curve 92CM-7091
5W6-GT						X			10-1-53	6W6-GT Tent. Data
				ł		X				Curve 92CM-7942
5W7-G	Ι,		ł	ļ		Х			12-1-41	6W7-G Data
5X4					H	X			10-1-53	6X4 Data 1
	l					X			10-1-53	Data 2
			l			X		1		Curve 92CM-8024
6X5, 6X5-GT			1	١.		X			3-20-43	Curve 92CM-8031 6X5, 6X5-GT/G Data
5X8				li		x			10-1-53	6X8 Data 1
0^0					-	â			9-1-52	Tent. Data 2
						â			9-1-32	Curve 92CM-7532
						x				Curve 92CM-7547R1
	١,					x				Curve 92CM-7844
5Y6-G						x			9-15-49	6Y6-G Data
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						x			J-1J-7J	Curve 92CM-6127R1
5Z4						11	ı			See 84/6Z4
5Z7-G						x			9-1-38	6Z7-G Tent. Data
5ZY5-G						x			12-1-41	6ZY5-G Data
7.44			ĺ			x			5-1-41	7A4 Tent. Data
7A5						-11	ļ	- 1	5-1-41	7A5 Tent, Data (on back of
						ĺ	- 1	ì		7A4 sheet
7A6 j					ΙÌ	Х			6-20-47	7A6 Data
7 <b>A</b> 7					Ì	**			6-20-47	7A7 Data (on back of 7A6 sheet)
7A8						Х			5-1-41	7A8 Data
7AD7	ı					Х			5-20-49	7AD7 Tent. Data
7AF7	ŀ			ı		X			6-15-48	7AF7 Data
7AG7						""			6-15- <del>4</del> 8	7AG7 Data (on <b>7AF7 sheet</b> )
7AH7	ļ					X			2-1-49	7AH7 Data
7B4	- 1					X			6-20-47	7B4 Data
7B5	ŀ					x	- 1		6-20-47	7B5 Data (on back of 7B4 sheet)
7B6		- 1				긺	1		6-20-47	786 Data
7B7						×	ł	ŀ	6-20-47	7B7 Data (on back of 7B6 sheet)
7B8		J			- 1	_^	- 1		6-20-47	788 Data 78P7-A Tent. Data
7BP7-A	- [	X					-	- 1	6-15-48	Outline CE-6367R3
7C5	ļ	^				.,		- [	6-13-48	7C5 Data (on back of 7B8 sheet)
7C6	- 1					×		-	4-15-40	7C5 Data (on back of 7B\$ sneet)
707	- 1					긲			5-15-40	7C7 Tent. Data (on back of 7C6 sheet
7C24	- [				- 1		ı		2., 2., 10	See 5762/7C24
7CP1		×		- 1	- [		- 1		8-15-46	7CP1 Data
	- 1	x		- [	-				8-15-46	Outline CE-6364R2
7DP4	ı	x			- [		- 1		11-15-49	7DP4 Data
	۱	Ϋ́	.	- 1			ı		10-15-47	Outline CE-6664R1A
	- 1	×	ļ	- [		1	- 1			Curve 92CM-6674R1



Tube Type	_	4DE								
Tube Type				_		_			CONT	ENTS
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	G	С	P	F	м	R	S	т	Date	Sheet
7E6						x			9-30-48	7E6 Data
7E7						X			9-30-48	7E7 Data
7F7					l	X			12-30-47	7F7 Data 7F8 Data
7F8						x			12-30-47	767 Data
7H7						x			12-30-47	7H7 Data
7,17	Į					X			12-30-47	7J7 Data
7JP1	- 1	x			1				1-1-51	7JP1 Tent. Data 1
	- 1	x							1-1-51	Tent. Data 2
7JP4	- 1	X	1						9-2-47	7JP4 Tent. Data
	ı	×	.		1				9-2-47	Outline CE-6667
		×				v		1	F 30 40	Curve 92CM-6888
7K7						X			5-20-49 10-15-47	7L7 Data
7L7		×				^			10-15-47	7MP7 Data
1MF1		â	l						10-1-51	Outline CE-7438R3
7MP14		x	1						10-1-51	7MP14 Data
7N7	ì								10-15-47	7N7 Data (on back of 7L7 sheet)
7NP4	ı	x			ļ				6-1-53	7NP4 Tent. Data 1
	]	x							11-1-50	Tent, Data 2
		x	1		1				11-1-50	Outline CE-7476B
		х	1							Curve 92CM-7515
7Q7						X			5-1-41	7Q7 Tent. Data
7QP4		X							1-1-51	7QP4 Tent, Data
		X							1-1-51	Outline CE-7524A Curve 92CM-7529
707	- 1	×				J		1	10-15-47	7R7 Data
7R7	- 1					X	ı		12-30-47	7S7 Data
7TP4	- {	×				^			2-1-52	7TP4 Tent. Data
/ / /		x				ı			2-1-52	Outline CE-7691
		x				l				Curve 92CM-7688
7V7	-				l	x			6-15-48	7V7 Data
7VP1		x							11-1-52	7VP1 Tent. Data 1
		X							11-1-52	Tent. Data 2
7W7	- 1					"	- 1		6-15-48	7W7 Data (on back of 7V7 sheet)
7WP4	ı	X							7-1-52	7WP4 Tent. Data 1
		X							7-1-52 7-1-52	Tent. Data 2 Outline Notes CE-7731
		×	ı						7-1-52	Curve 92CM-7515
7X7		^				x			3-15-48	7X7 Data
7Y4		- 1			- 1	٠			12-30-47	7Y4 Data
7Z4	ļ		l	1	- 1	- îi			12-30-47	7Z4 Data (on back of 7Y4 sheet)
8D21	- 1	-	.					x	9-30-48	8D21 Data 1
	-				- 1			X	9-30-48	Data 2
							i	x	9-30-48	Data 3
	- 1							×	9-30-48	Outline Details CE-6687V2B
		ļ						X		Curve 92CM-6989
9C21		- 1			1	- 1				9C21 Data 1
						- 1			10-15-47	
	- 1	- 1	1			- 1		X	1	Curve 92CM-6457
	- 1		- 1	ļ		- 1		XI		Curve 92CM-6458 Curve 92CM-6462
,	ı	,	ı	-	1	ı		^1	'	Curve 92CM-0402



	- 11	4DE	A ~						CONT	ENTS
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Tube Type	G	C	P	Sec	tion M	Ŕ	s	T	Date	Sheet
9C22	H		$\vdash$	Н	$\dashv$	-	_	×	10-1-51	9C22 Data 1
JC22								х	10-1-51	Data 2
			1		. 1			х	10-1-51	Outline CE-6447R2-6519
C25	1				1			х	8-15-46	9C25 Tent. Data 1
JCL5					H			x	5-20-49	Data 2
		l						x	8-15-46	Outline CE-6750
						1		x	0 .,	Curve 92CM-7269
			1					x		Curve 92CM-7234
OBP4		x							3-15-48	10BP4 Data
	1	x		1	l			l	10-15-47	Outline CE-6663R2A
	l	x		1	1			l	,,	Curve 92CM-6675R2
10BP4-A		x			ΙI				5-1-50	10BP4-A Data
	i	x							5-1-50	Outline CE-6663R3A
		x	1	1	1			ĺ	5-1-50	Curve CE-7448
	1	Ιx	1	1					3-1-50	Curve 92CM-7454
10FP4-A	1	x	1						8-1-51	10FP4-A Tent, Data
		lх		l					8-1-51	Outline CE-7629
IOKP7	1	×						1	9-30-48	
	1	x		İ	li		1	l	9-30-48	Outline CE-6932
IOSP4	1	Ιx						ł	7-1-52	10SP4 Tent, Data
	1	x	1	1	1			l	7-1-52	Outline CE-7729
	1	x	1		1 !		1		/-1-52	Curve 92CM-7773
10-Y				ŀ			l	l x	12-20-46	
2A6		1		ļ	x		l	1	5-1-42	12A6 Tent. Data
D.O	ì	1	l	ļ	ľx			Ì	3-12	Curve 92C-6327
12A7	ł		1	1	1	x	1		8-2-43	12A7 Data
12A8-GT	1		1		1	î			8-2-43	12A8-GT/G Data (on 12A7 sheet)
12AH7-GT							t	ı	8-2-43	12AH7-GT Data
274111-01				ļ.					0-2-43	(on back of 12A7 shee
12AL5	1	ļ				x	ı	1	6-20-47	12AL5 Tent. Data
12AQ5	1	1		1		x	l	1	8-1-53	12AQ5 Tent. Data 1
12.63	1	1		1	1	Îx.	l		8-1-53	Tent. Data 2
12AT6	1		į.	1	i		1	1	6-20-47	12AT6 Data (on back of 12AL5 shee
12AT7		1 .		1	1	×	1		2-1-49	12AT7 Tent. Data
12/11/		1			1	x	1	1	2-1-77	Curve 92CM-7056
174116	1	1		1	l	î			2-1-49	12AU6 Data (on back of 12AT7
12AU6	1	1		1	1	1			2-1-49	Curve 92CM-705
12AU7	1	]	1		1	×	1		12-20-46	
		1	1			Iŵ.		ì	10-15-47	12AV6 Data
12AV6 12AW6		1	1			Î	ı	1	4-15-47	12AW6 Tent, Data
12AW6			!	1		ı,	ı		4-13-47	Curve 92CM-6855
124V4 CT	1	1		1	1	Iî.	ı	1	9-1-52	12AX4-GT Tent, Data
12AX4-GT	1	1		1		lî.	1		9-15-47	12AX7 Tent. Data
12AX7			ŀ		1	lî.	1		3-13-47	Curve 92CM-6879
1247	1		1	l	1	^	1	1	4 1 52	
12AY7	1		1	1	X	1	1		4-1-53	12AY7 Tent. Data Curve 92CM-7861
	1	1	1	1	١^	١.,	1	1	1	
12BA6	1	1	1	1	1	X	1	1	11-1-52	
12BA7		1		1	1	1::	1	1	11-1-52	12BA7 Data (on 12BA6 sheet)
12BD6		1	1	1	1		1		11-1-52	12BD6 Data (on 12BA6 sheet)
12BE6	1	1	1	1		1	ı	1	11-1-52	12BE6 Data (on 12BA6 sheet)
12BF6	1	1	1	1		"	ı		11-1-52	
128H7	1	1	1	1		×	ı	1	5-1-52	128H7 Tent. Data Curve 92CM-7742



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,	_		_						CONT	rents
				Sec	ction					
Tube Type	G	C	P	F	м	R	s	T	Date	Sheet
12C8						×	i		9-15-49	12C8 Data
12DP7-B		×							9-1-52	12DP7-B Tent. Data
		×							9-1-52	Outline CE-6375R5
12F5-GT									9-15-49	12F5-GT Data (on 12C8 sheet)
12H6									9-15-49	12H6 Data (on 12C8 sheet)
12J5-GT		:			ĺ				9-15-49	12J5-GT Data (on 12C8 sheet)
12J7-GT									9-15-49	12J7-GT Data (on back of 12C8 shee
12K7-GT									9-15-49	12K7-GT Data
1287-01									7-13-77	(on back of 12C8 shee
12K8			l			,,			9-15-49	12K8 Data (on back of 12C8 sheet)
12KP4-A		×					1		8-1-51	12KP4-A Tent. Data
12057-0		Î							8-1-51	Outline CE-7630
12L8-GT		^	ĺ		x				10-1-43	12L8-GT Data
12LP4		×			^				9-15-49	12LP4 Tent, Data
		x							9-15-49	Outline CE-7276
	1	lα	l						3-13-12	Curve 92CM-7310
12LP4-A		x	l						5-1-50	12LP4-A Data
		x			!	'			5-1-50	Outline CE-7276R2
		X	1		1					Curve 92CM-7453
12Q7-GT		1							9-15-49	12Q7-GT Data
				1		1		l		fon back of 12C8 shee
1258-GT	1		1	i	l	x			9-15-49	12S8-GT Data
12SA7.	1					,				
12SA7-GT	1			1		11			9-15-49	12SA7, 12SA7-GT Data
	1		l	1	1					(on 1258 GT shee
12SC7				1		"		1	9-15-49	12SC7 Data (on 12S8-GT sheet)
12SF5,	l		i							
12SF5-GT		l	ŀ	l	ł	11	ŀ		9-15-49	12SF5, 12SF5-GT Data
	l				l					(on 1258-GT shee
12SF7	1	l				"			9-15-49	12SF7 Data
	1			l						(on back of 1288-GT shee
12SG7			1			"	1		9-15-49	12SG7 Data
					i			1	Ì	(on back of 1258-GT shee
12SH7				ı	1	*1			9-15-49	12SH7 Data
		1		1	ŀ			l		(on back of 1258-GT shee
12SJ7,		1			E	١		İ		
12SJ7-GT		1			1	"			9-15-49	
		1			i					(on back of 1258-GT shee
12SK7,			1		l	L		ŀ		10047 10047 07 0
125K7-GT					1	X.			10-1-53	12SK7, 12SK7-GT Data
12SL7-GT	1	1	-			;;			10-1-53	12SL7-GT Data (on 12SK7 sheet)
125N7-GT	1	L			1	١''	1		10-1-53	12SN7-GT Data (on 12SK7 sheet)
12SP7	ł	X	1						8-1-51	12SP7 Tent, Data
17507	1	ľ	I					1	8-1-51	Outline CE-7598
12SQ7, 12SQ7-GT	1		I		1	١.,		1	1015	13507 13507 CT D-4-
12301-01	1		1			Ι"			10-1-53	12SQ7, 12SQ7-GT Data (on 12SK7 shee
12\$R7			1			١.,		İ	10-1-53	12SR7 Data (on back of 12SK7 sheet)
12SW7	ì		1		\ \		ŀ	1	6-20-46	12SW7 Tent, Data
12SX7-GT	1	1	1	ĺ	10	Ĺ	1	1	6-20-46	12SX7-GT Tent, Data
123/1-01	I		i		×××	ı			0-20-46	Curve 92CM-6782
	1	1	1	1	1~		1	•		Cuive 72C/VI-0/62



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Tube Type	G	c	P	Sec	ction M	R	S	Ŧ	Date	Sheet
12SY7					×				6-20-46	12SY7 Tent. Data Curve 92CM-6786
12V6-GT						"			10-1-53	12V6-GT Data (on back of 12SE7 sheet
12X4 12Z3 14A4						×			10-1-53 2-2-40 12-30-47	12X4 Data (on back of 12SK7 sheet) 12Z3 Data
14A5 14A7						:			12-30-47 12-30-47	14A5 Data (on 14A4 sheet) 14A7 Data (on back of 14A4 sheet)
14AF7 14B6 14B8						X ::			11-15-48  11-15-48  11-15-48	1486 Data (on back of 14AF7 sheet)
14C5 14C7						×			11-15-48 11-15-48	14C5 Data (on back of 14AF7 sheet) 14C7 Data
14CP4		X X X							8-1-51 8-1-51	14CP4 Tent. Data . Curve 92CM-7625 Outline CE-7631B
14E6 14E7 14EP4		×				::			11-15-48 11-15-48 3-1-51	14E7 Data (on back of 14C7 sheet) 14EP4 Tent, Data 1
		x x							3-1-51 3-1-51	Tent. Data 2 Outline CE-7554R2B Curve 92CM-7567
14F7 14F8 14H7						::			11-15-48 11-15-48 11-15-48	14F8 Data (on back of 14C7 sheet) 14H7 Data (on back of 14C7 sheet)
14J7 14N7 14Q7						X			5-1-50 5-1-50 5-1-50	14J7 Data 14N7 Data (on 14J7 sheet) 14Q7 Data (on 14J7 sheet)
14R7 16ADP7		×			İ	"			5-1-50 2-1-52 2-1-52	14R7 Data (on 14f7 sheet) 16ADP7 Tent. Data Outline CE-7690
16AP4-A		X							5-1-50 5-1-50	16AP4-A Data Outline CE-7449A Curve 92CM-7471
16DP4-A 16GP4		× ×							2-1-52 7-3-50 2-1-50	16DP4-A Tent. Data 16GP4 Tent. Data RefLine Gauge CE-7391
16GP4-A		×							7-1-52 7-1-52	Curve 92CM-7351R1 16GP4-A Data 16GP4-B Data (on 16GP4-A sheet)
16GP4-C		::		İ					7-1-52 7-1-52 7-1-52	16GP4-C Data (on 16GP4-A sheet) 16KP4 Data
16LP4-A		×××							2-1-52 8-1-51 8-1-51	(on back of 18GP4-A sheet 16LP4-A Tent, Data 16RP4 Tent, Data 1 Tent, Data 2
16TP4		×××							8-1-51 8-1-51	Outline CE-7627B Curve 92CM-7623 16TP4 Tent. Data 1
		×××							8-1-51 8-1-51	Tent. Data 2 Outline CE-7632B Curve 92CM-7628



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16WP4-A	┪	x		-		Н	_	Н	2-1-52	16WP4-A Tent, Data
17BP4-A		Ω							5-1-51	17BP4-A Tent, Data
.,	ı	x							2 . 2.	Curve 92CM-7595
	- 1	χl							5-1-51	Outline CE-7589B
17CP4		x	1						1-1-51	17CP4 Tent, Data
,,,,,,,,,,,		Ω							1-1-51	RefLine Gauge CE-7391
		x							1-1-51	Outline CE-7535B
l		×								Curve 92CM-7533
17GP4	1	x						П	5-1-51	17GP4 Tent. Data 1
	- 1	x							5-1-51	Tent, Data 2
	- 1	x	i						5-1-51	Outline CE-7601B
	- 1	x								Curve 92CM-7606
17HP4	- 1	x							2-1-52	17HP4 Tent. Data 1
	- 1	x							2-1-52	Tent, Data 2
		x							2-1-52	Outline CE-7686B
[	-	X								Curve 92CM-7685
17JP4	- 1	х							7-1-52	17JP4 Tent, Data
	ĺ	x						- 1		Curve 92CM-7753
	- 1	x				1		l	7-1-52	Outline CE-7745R2B
1	- 1	х								Curve 92CM-7652R1
17LP4	-	х							7-1-52	17LP4 Tent. Data 1
		x				1		1	7-1-52	Tent, Data 2
ŀ	- 1	х							7-1-52	Outline CE-7710R1B
		x			Ιi	li				Curve 92CM-7702R1
17QP4	- 1	x					'		7-1-52	17QP4 Tent. Data 1
		X		1					7-1-52	Tent. Data 2
1		x							7-1-52	Outline CE-7734R1B
i		X								Curve 92CM-7755
17TP4	- 1	x							10-1-51	17TP4 Tent, Data 1
	- [	х							10-1-51	Tent, Data 2
	i	х							10-1-51	Outline CE-7601R1B
	- 1	x								Curve 92CM-7606
19	- 1					х			4-20-38	19 Data
19AP4		x							3-1-51	19AP4 Data
19AP4-A	- 1	-11							3-1-51	19AP4-A Data (on 19AP4 sheet)
19AP4-B	- 1	x	ı					1	9-1-50	19AP4-B Tent, Data
	- 1	X							9-1-50	Outline CE-7502R1
	- 1	X	- 1							Curve 92CM-7506
19AP4-D	- 1	X	ļ	.					3-1-51	19AP4-D Data
19BG6-G						х			9-1-50	19BG6-G Tent. Data
19J6						Х			11-15-48	19J6 Tent. Data
						X		ı		Curve 92CM-7061
19T8						X			9-1-52	19T8 Data
19X8	- 1	-				"			9-1-52	19X8 Data (on 1978 sheet)
20CP4	- [	x							5-1-51	20CP4 Tent. Data 1
	- [	x							5-1-51	Tent. Data 2
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		X								Curve 92CM-7616
20MP4		хl	- 1						5-1-52	20MP4 Tent. Data
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		хl							5-1-52	Outline CE-7722B
l		x								Curve 92CM-7723



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35A5						X			6-20-47	35A5 Data
35B5					ll	X			12-20-46	
				İ	l	X				Curve 92CM-6312R1
35C5		1				X		Ιİ	3-15-48	35C5 Tent, Data
35L6-GT		-				×			6-20-47	35L6-GT Data
				ĺ		X		Ιí		Curve 92CM-6309
25344						×			0 1 50	Curve 92CM-6307R1
35W4					ΙI				9-1-50	35W4 Data
2574						×			12 20 47	Curve 92CM-6615R1
35Y4 35Z3						â			12-30-47 6-20-47	35Y4 Data 35Z3 Data
35Z4-GT					ΙI	::1			6-20-47	35Z4-GT Data (on back of
3)27-01				Ι.		- 1			0-20-47	35Z3 she
35Z5-GT	- 1					x			6-1-43	35Z5-GT/G Doto
36						â۱	- 1		8-20-35	36 Data
37						Ω			11-1-37	37 Data
38						î۱	ŀ		4-3-39	38 Data
39						Ω			11-1-37	39/44 Data
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42						$\hat{\mathbf{x}}$	- 1		4-20-38	42 Data
43						$\hat{\mathbf{x}}$	-		6-1-37	43 Data
44	i					11	- 1		• . • .	See 39/44
45						x	ĺ		4-20-38	45 Data
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45Z5-GT						x			1-30-42	45Z5-GT Data
46					l	x			7-1-38	46 Data
47						x	- 1	l	11-1-37	47 Data
50A5		i				X	- 1		12-30-47	50A5 Data
50B5					ļ	X	- 1		1-2-46	50B5 Tent. Data
ĺ					- 1	X	- 1			Curve 92CM-6603
50C5					- 1	X	- 1		3-15-48	50C5 Tent, Data
50C6-G						X)	- 1		2-1-50	50C6-G Data
50L6-GT	1					X	- 1		9-2-41	50L6-GT Data
	- 1					X	- 1			Curve 92CM-6314R1
50X6					- 1	X			2-1-50	50X6 Data
50Y6-GT						**			2-1-50	50Y6-GT Data
					l	1				(on back of 50X6 she
50Y7-GT						X			2-1-50	50Y7-GT Data
50 <b>Z7-G</b>	1					X	- 1		8-2-43	50Z7-G Data
53 <i>.</i>	-					X	- 1		4-5-37	53 Data
55	1					Χl	- 1		6-15-48	55 Data
56	-					"	- 1		6-15-48	56 Data (on 55 sheet)
57	ļ						- 1		6-15-48	57 Data (on 55 sheet)
58	- 1						ı	l	6-15-48	58 Data (on back of 55 sheet)
59	-					X			12-20-38	59 Data
7017 67						X	ı	۱ ا	,, , ,.	Curve 92S-5193R1
70L7-GT						X		F	12-1-41	70L7-GT Data
., .						X	- 1			Curve 92C-6324
71-4						X	-		7-1-35	71-A Data
75					]	×	- 1	-	9-2-41	75 Data
VR75-30			H	- 1	- 1	- 1	- 1	- 1	1	Superseded by 0A3/VR75

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83						11			9-2-41	83 Data (on back of 82 sheet)
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117P7-GT				ŀ		×			12-1-41	117L7-GT/117M7-GT shee 117P7-GT Tent. Data
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117Z3		1				Î.			7-3-50	117Z3 Data
117Z4-GT					ļ	î			2-1-49	117Z4-GT Data
117Z6-GT						x.			8-2-43	117Z6-GT/G Data
VR150-30			1		Į	, ·			0-2-43	Superseded by 0D3/VR150
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	l							x	9-30-48	Data 2
		l						x	9-30-48	Shell No. 3906 (CE-7020
						ŀ		X		Curve 92CM-4551
	ļ				ì	1	l	X		Curve 92CM-5551
211	i	İ	ŀ	ŀ				X	5-1-50	211 Data 1
	l	l						X	5-1-50	Data 2
		ł					į	X		Curve 92CM-4537
217-C			ļ					X	6-20-47	217-C Data
502-A			1	X					9-30-48	502-A Data
,				×	ĺ				9-30-48	Curves CE-7074T - 7072T
559					X				11-15-45	559 Tent. Data
				l	X					Curve 92CM-6588
575-A		ŀ						×	5-1-46	575-A Tent. Data
579-B				١	X				5-1-46	579-B Tent. Data
627		1		X.					5-1-46	627 Tent. Data
629	1	1		X					5-1-46	629 Tent. Data
672-A			ŀ	×			ĺ	١.	6-1-48	672-A Tent. Data
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								X	8-1-51	Data 3
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								X		Curve 92CM-4678
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	П								12-20-46	Data 2
								X		Curve 92CM-4836
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								X	5-20-49	Curve 92C-4981
311-A								X	5-20-49	811-A Data 1 Data 2
								x	5-20-49	Outline CE-6905
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312-A		ļ		- 1				x	3-1-51	Tent. Data 2
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									5-20-49	Data 2
								x	5-20-49	Data 3
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					- 1	-		x		Curve 92CM-4968R1
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# RCA PREFERRED TUBE TYPES FOR NEW EQUIPMENT DESIGN

This list of Preferred Tube Types is presented to assist equipment manufacturers in formulating their plans for future production of electronic equipment. It is based on a careful survey of the needs of the engineering and manufacturing fields.

The soundness of the Preferred Tube Program, first introduced by RCA in January, 1940, has been proven with the passing years.

By using Preferred Tube Types, electronic-equipment manufacturers can reduce manufacturing costs for the following reasons:

- I. LOWER INITIAL
  COST OF TUBES
- a. We can manufacture more efficiently for stock.
- b. Our production rate on preferred types is more uniform because of smaller demand for other types.
- 2. MORE PROFIT
  THROUGH BETTER
  DELIVERIES
- Fewer tube types mean better deliveries and insure continuous production of electronic equipment.
- 3. IMPROVED QUALITY
  OF PRODUCT FROM
  LONGER PRODUCTION RUNS
- a. Tube operator acquires more skill working on one type for a considerable length of time. Such skill results in better quality which means less cost to equipment manufacturers on their production line because of fewer stoppages.
- 4. STANDARD!ZATION
  OF FENER TUBE
  TYPES
- Permits standardizing fewer accessory parts, such as capacitors, resistors, etc.
- TYPES
- Results in purchasing and stocking economies.
- 5. CUSTOMER SATISFACTION
- a. Purchasers of electronic equipment equipped with Preferred Type Tubes will have greater satisfaction, we believe, because these fast-moving types can be regularly stocked and will, therefore, be easier to obtain for renewal purposes.

This list, of course, is subject to change resulting from technological advances in tube design and application. When such changes become necessary, they will be incorporated in revised issues of this list.



Miniature Types are shown in italics

#### VACUUM TYPES FOR RE AND AF POWER APPLICATIONS

Values shown are Unmodulated Class C Ratings

for Continuous Commercial Service

TYPE	CLASS	М	AXIMUM I	NPUT PO	WER vs F	REQUENCY	1	UNITS
ITPE	CLASS	1.6	7.5	15	25	50	75	Mc
5763	Beam	15	15	15	15	15	15	watts
2E24	Beam	30	30	30	30	30	30	watts
2E26	Beam	30	30	30	30	30	30	watts
832-A	Beam	36	36	36	36	36	36	watts
807°	Beam	60	60	60	60	50	40	watts
6146°	Beam	67.5	67.5	67.5	67.5	67.5	63	watts
829-B°	Beam <sup>D</sup>	120	120	120	120	120	120	watts
812-A°	Triode	175	175	175	175	160	130	watts
811-A* 8005* 4X150A 813*	Triode Triode Tetrode Beam	175 240 250 360	175 240 250 360	175 240 250 360	175 240 250 360	160 195 250 300	130 250	watts watts watts watts
6161 8000 <sup>©</sup> 4–125A/	Triode Triode	400 500	400 500	400 500	400 500	400 400	400 300	watts watts
4D21	Tetrode	500	500	500	500	500	500	watts
5786	Triode	1.5	1.5	1.5	1.5	1.5	1.5	kw
833-A*	Triode	1.8	1.8	1.8	1.75	1.5	1.2	kw
6181	Tetrode	2.5	2.5	2.5	2.5	2.5	2.5	kw
5762	Triode	8.7	8.7	8.7	8.7	8.3*	7.9*	kw
889R-A	Triode	16	16	16	16	12	9.6	kw
6166	Tetrode	18	18	18	18	17.8†	17.7†	kw
892	Triode	30	22.5	17	-	-	-	kw
5771	Triode	67.5	60	60	60	45	-	kw
5671	Triode	100	100	90	80	-	-	kw
5770	Triode	150	150	150	135	-	-	kw

Twin Type - Input values per tube for push-pull operation.

#### **THYRATRONS**

#### IGNITRONS

#### RECTIFIERS®

2D21 672-A 2050 6012	5560 5563 5696
-------------------------------	----------------------

2X2-A 857-B 3B28 866-A 5R4-GY 869-B 673 8008
---

For additional vacuum—type rectifiers, see listing of types for Receiver Applications.

Type may be operated at higher ratings in Intermittent Commercial and Amateur Service (ICAS) as given in published data for each type.

<sup>★</sup> For Television Picture Service over the range of 54 Mc. to 216 Mc., the CCS maximum rated input power is 6.5 kw.

<sup>1</sup> For Television Picture Service over the range of 54 Mc. to 216 Mc., the CCS maximum rated input power is 22 kw.



Miniature Types are shown in italics

#### VACUUM TYPES FOR RF AND AF POWER APPLICATIONS: (Cont'd)

Values shown are Immodulated Class C Ratings for Continuous Commercial Service

			UT DONES	- FREQUEN	av	· · · · · · · · · · · · · · · · · · ·	T
UNITS	MA	XINUM INP				CLASS	TYPE
Mc	110	175	220	450	900		
watts watts watts watts watts watts watts watts watts	15 30 30 36 - 56 120	15 20 20 36 - 47 120	- - 34 - - 114	-	-	Beam Beam Beam Beam Beam Beam Beam	5763° 2E24° 2E26° 832-A° 807° 6146° 829-B°
watts watts watts watts watts watts watts watts	- - 250 - 400	250 - 400	- - 250 - 400	250 - 400	- - - - 400	Triode Triode Triode Tetrode Beam Triode Triode	812-A <sup>®</sup> 811-A <sup>®</sup> 8005 <sup>®</sup> 4X150A 813 <sup>®</sup> 6161 8000 <sup>®</sup>
watts kw kw kw kw kw kw kw kw kw kw kw	500 1.5 - 2.5 7.3* - 17.2†	470 1.5 - 2.5 6.1* - 16.5†	390 - 2.5 4.5* - 16 - -	2.55	2.5	Tetrode Triode Triode Triode Triode Triode Triode Triode Triode Triode Triode Triode Triode Triode	4-125A/ 4D21 5786 833-A* 6181 5762 889R-A 6166 892 5771 5671 5770

# SMALL TYPES FOR INDUSTRIAL AND COMMUNICATION SERVICES

	NTERTAINMENT TYPES PECIAL INTEREST*	VACUUM TYPES FOR CRITICAL APPLICATIONS	TYPES FOR REGULATOR SERVICE	GLOW DISCHARGE TRIODE
6AK6 6AQ6 6BJ6 6C4	6L6-G 6SC7 6SL7-GT 12 <b>AI</b> 7 <sup>▲</sup>	1620 5690 5691 "Special Red" 5692 Types 5693 5879	0 A2 0 B2 5651 6080	5823

<sup>\*</sup> Also see types for AM, FM, & TV Receivers.

<sup>▲</sup> Tapped heater, for 6.3-volt or 12.6-volt operation.



Miniature Types are shown in italics

#### TYPES FOR AM AND FM BROADCAST RECEIVER APPLICATIONS

RECTIFIERS		AMPLIF					
an d	CONVERTERS	FRTERS Tric		Pentodes			OUTPUT
DIODE DETECTORS		Twin	With Diodes	Shårp Cutoff	Remote Cutoff		AMPLIFIERS
	1R5			14	1T4	185	3S4
5U4-G 5Y3-GT 6AL5	6 <i>BE</i> 6 6 <b>X</b> 8		6AV6	6AU6 6CB6	6BA6		3 <b>V</b> 4 6 <b>AQ5</b> 6K6–GT 6V6–GT
6 <b>1</b> 4 35 W4	12BE6	12407▲	12AV6		12BA6		35°C5 50°C5

#### TYPES FOR TELEVISION RECEIVER APPLICATIONS

RF TUNER Tubes	AMPLIFIERS				SOUND 4	
	l F	Video	Audio	Deflection	DEFLECTION OSCILLATORS	VIDEO DETECTOR
6AF4* 6BQ7-A* 6J6 6X8	6AU6 6BQ7-A 6CB6	6AU6 6CL6	6AQ5 6AV6 6K6-GT 6V6-GT	6S4 6BQ6-GT 6CD6-G 6W6-GT	6SN7-GT 12AU7♣	6AL5
					12NU7- 12BH7▲	

RECTIFIERS			
High- Voltage	Low- Voitage	DAMPER Tube	CONTROL CIRCUITS
1B3GT	5U4-G	6AX4-GT 6W4-GT	6AU6 6SN7-GT
			12AU7▲ 12BH7▲

<sup>\*</sup> For UHF.

<sup>▲</sup> Tapped heater, for 6.3-volt or 12.6-volt operation.

<sup>♠</sup> Including synchronizing functions, AGC, etc.



Miniature Types are shown in italics

#### C-R OSCILLOGRAPH TYPES

P   Screen	P7 SCREEN	PII SCREEN	PI4 SCREEN	P16 SCREEN
2BP1 3JP1* 3RP1 .	3JP7*	2BP11 3KP11		
5ABP1* 5UP1	5ABP7* 5FP7-A 5UP7	5ABP11* 5UP11 5WP11*	5FP14	5ZP16 <sup>3</sup>
	7MP7 10KP7 12SP7 16ADP7		7MP14	32/10

<sup>↑</sup> Transcriber Type

#### **PHOTOTUBES**

SINGLE	MULTIPLIER	
S I Response	34 Response	S4 Response
1P40 921 922 927	1P39	931-A 5819 6199

#### CAMERA AND TV STUDIO TYPES

5820	Image Orthicon
6198	Vidicon <sup>D</sup>
2F21	Monoscope

ndustrial Type

Flying-Spot Type

<sup>\*</sup> Post-Deflection Accelerator Type



# RCA TUBE TYPES NOT RECOMMENDED FOR NEW EQUIPMENT DESIGN

Certain tube types should be avoided in the design of new equipment because they are approaching obsolescence or have limited or dwindling demand. Such RCA types are listed below for the benefit of equipment designers.

	RECEIVING TUBE TYPES				
0Z4-G 1A5-GT 1C5-GT 1D8-GT 1G6-GT 1LA4 1Q5-GT 1S4 1T5-GT 1-v 5T4 5W4-GT 5X4-G 5Y4-G 5Y4-G 5Y4-G 5Y4-G 6A3 6A7 6A8	6A8-G 6A8-GT 6A85/6N5 6A87 6AC5-GT 6AF6-G 6B8 6C6 6C8-G 6D6 6F5 6F5-GT 6F6-G 6F7 6G6-G 6H6-GT 6J7-GT 6J8-G 6K7	6K7-G 6K7-GT 6K7-GT 6Q7-GT 6Q7-GT 6S7-GSA7-GT 6SB7-Y 6SF7-GT 6SQ7-GT 6SS7 6ST7 6ST7 6U7-G 6X5 7E7	14C5 14H7 24-A 25A6 25W4-GT 25Z5 25Z6 26 27	45 47 56 57 58 70L7GT 71-A 75 76	
	TRANSM	ITTING TUBE	TYPES		
10-Y 203-A 207 211 217-C 800	801-A 803 804 830-B 838 841	842 843 846 849 851 860	861 862-A 865 893-A 893A-R 898-A	1619 1623 1624 1626 8012-A	

# CATHODE-RAY TUBE TYPES

2AP1-A	10FP4-A	16KP4	16TP4	905-A
3AP1-A	12KP4-A	16LP4-A	16WP4-A	908-A
3KP4	14CP4	16RP4	902-A	913
5BP1-A	16DP4-A			

(continued on next page)



# RCA TUBE TYPES NOT RECOMMENDED FOR NEW EQUIPMENT DESIGN

РНОТО	TUBES	THYRAT	RONS
923	924	629	885

#### MISCELLANEOUS

2A4-G	2V3-G	874
2C21/1642	559	878
2022	864	1634



POWER TUBES, RECTIFIER TUBES, THYRATRONS, IGNITRONS, VOLTAGE REGULATORS, PHOTOTUBES, CATHODE-RAY TUBES, AND SPECIAL TYPES

Where an RCA Type Number is followed by an asterisk (\*), this type is not directly interchangeable, but is in the same general class.

TYPE RCA NUMBER NUMBER	TYPE RCA NUMBER NUMBER
CE-I A/B,C,D 868, 918 CE-IV A/B,C,D 917*, 919* IP32 927* CE-2 A/B,C,D	CE-23 A/B,C,D 923 PJ-23
284	FG-27A 5559*
38P1	CE-28 A/8,C,D 928 RK-28 803 RK-28A 803 CE-29 A/B,C,D 929, P39 CE-30 A/B,C,D 930, P40
CE-5 A/B,C,D	FG-32 5558 RK-33 2C21/1642
6Q5G 884 7GP4 7JP4 PJ-8 5556 G-9 868	CE-34
CE-11V A/B, C, D	RK-37 . 808* RK-38 . 806* RK-39 807 HY-40 . 812-A* HY-40Z . 811*
FG-17.     5557       CE-20.     927       FV-20.     8000*       RK-20A     804       T-20.     1623*	T-40
CE-21 A/B,C,D 920	
• Except in high-altitude service.	



SEPT. 30, 1948



TYPF RCA	TYPF	RCA
1 =		
NUMBER NUMBER	NUMBER	NUMBER
WE-2548 865*	WE-331	805*
WE-2558	WE-341AA	891-R*
HK-257B 4E27/8001	UE-342B	211
FG-258A 5553	C-350	807*
HF-258B 866-A*	353A	
FG-259B		
260A 860*	HK-354 C, D, E, F	806*
HF-261A 835*	WE-356A	
264 A,B 864*	WE-357A	
266B 857-B*	F-357A	857-B*
WE-266C 857-B*	F-363A	892*
267B 872-A*	F-367A	673*
WE-268A 801-A*	375-A	575-A
FG-271 5551	F-376A	835*
WE-271A 843*	393A	3C23*
WT-272 5557	FJ-401	IP29
WE-274 A.B 5R4-GY*	GL-415	5550
276A 835*	GL-451	8020
282A 850*	UE-468	8000*
WE-284 A,D 845*	WL-463	806*
WE-287A 5557*	WL-471	8003*
WE-289A 4826/2000	WL-630	2050
WE-298A	WL-631	5559
WT-294	WL- 632A	5560
WE-295A 203A	KU-634	677
HF-300 806*	WL-651/656	5552
	WL-652/657	
UE-303A 203-A	WL-653B	5551
T-303C 8000*	WL-655/658	5555
UE-303U 8000		5553 672 A
UE-304A 204-A*	672	
WE-304B 834		5554
F-307A 207	WL-681/686	5550
WE-307A 837*	NL-715	5557
CE-309 5557	WL-734	917*
UE-310 801-A*	WL-735	868
CE-311 3C23	WL-74!	923*
UE-311 211	T-756	809*
UE-311C 835	801	80 I-A
UE-311CH 8000*	UE-812H	8005*
UE-311 T.CT 8003*	T-814	806*
UE-312E 849*	T-822	806*
315A 673*	825	1623*
UE-317C 217-C	829	829-B
WE-319A 872-A*	829-A	829-B
WE-321A 673*	832	832-A
WE-322A 803	833	833-A
"L- 522h		,
(continued on	following page)	

INTERCHANGEABILITY 2 SEPT. 30, 1948 TUBE DEPARTMENT INTER



TYPE RC	
1	1
F-857A	7-B UE-967
866 866	
869-A	2-A 1850-A 1850-A 1850-A
879 2X2 889 889	2-A 2051 2050 2-A 2501-A3
	10001
UE-911CH 83 914 914	B-A 8016

When operated under 8014-A conditions, can replace 8014-A.

Where a "type to be replaced" carries a multiple designation incorporating a 5500-series number, that type can be directly replaced by the RCA type having the same 5500-series number. For example: the 5557/FG-17, as well as the FG-17, is directly replaceable by the RCA-5557. Likewise, the 5552/651/656, as well as the WL-651/656; is directly replaceable by the RCA-5552.



Amplification Factor  $(\mu)$  is a special case of mufactor. It is the ratio of the change in plate voltage to a change in control-electrode voltage under the conditions that the plate current remains unchanged and that all other electrode voltages are maintained constant. It is a measure of the effectiveness of the control-electrode voltage relative to that of the plate voltage upon the plate current. The sense is usually taken as positive when the voltages are changed in opposite directions. As most precisely used, the term amplification factor refers to infinitesimal changes.

Class A Amplifier: \* An amplifier in which the grid bias and the alternating grid voltages are such that plate current in a specific tube flows at all times.

1E69

The ideal class A amplifier is one in which the alternating component of the plate current is an exact reproduction of the form of the alternating grid voltage, and the plate current flows during the 360 electrical degrees of the cycle. The characteristics of a class A amplifier are low efficiency and output.

Class AB Amplifier:\* An amplifier in which the grid bias and alternating grid voltages are such that plate current in a specific tube flows for appreciably more than half but less than the entire electrical cycle.

1E70

The characteristics of a class AB amplifier are efficiency and output intermediate to those of a class A and a class B amplifier. The idle plate current and attendant dissipation may be made substantially less than is possible with class A amplifiers. This amplifier has been called class A prime.

<sup>■</sup> Definitions taken from the 1933 Report of the Standards Committee of the I.R.E. are followed by the definition number in the report.

<sup>\*</sup> To denote that grid current does not flow during any part of the input cycle, the suffix 1 may be added to the letter or letters of the class identification. The suffix 2 may be used to denote that grid current flows during some part of the cycle.



(continued from preceding page)

Class B Amplifier:\* An amplifier in which the grid bias is approximately equal to the cutoff value so that the plate current is approximately zero when no exciting grid voltage is applied and so that plate current in a specific tube flows for approximately one half of each cycle when an alternating grid voltage is applied.

1E71

The ideal class B amplifier is one in which the alternating component of plate current is an exact replica of the alternating grid voltage for the half cycle when the grid is positive with respect to the bias voltage, and the plate current flows during 180 electrical degrees of the cycle. The characteristics of a class B amplifier are medium efficiency and output.

Class C Amplifier: \* An amplifier in which the grid bias is appreciably greater than the cutoff value so that the plate current in each tube is zero when no alternating grid voltage is applied, and so that plate current in a specific tube flows for appreciably less than one half of each cycle when an alternating grid voltage is applied.

1E72

Class C amplifiers find application where high platecircuit efficiency is a paramount requirement and where departure from linearity between input and output is permissible. The characteristics of a class C amplifier are high plate-circuit efficiency and high power output.

Control-Grid—Plate Transconductance  $(g_m)$  is the name for the plate-current-to-control-grid-voltage transconductance. This is ordinarily the most important transconductance and is commonly understood when the term "transconductance" is used.

1E56

Formerly it was known as mutual conductance. See definition of Transconductance.

Conversion Transconductance (g<sub>c</sub>) is the quotient

<sup>·</sup> See preceding page.



(continued from preceding page)

of the magnitude of a single beat-frequency component  $(f_1 + f_2)$  or  $(f_1 - f_2)$  of the output-electrode current by the magnitude of the control-electrode voltage of frequency  $f_1$ , under the conditions that all direct electrode voltages and the magnitude of the electrode alternating voltage  $f_1$  remain constant and that no impedances at the frequencies  $f_1$  or  $f_2$  are present in the output circuit. As most precisely used, the term refers to infinitesimal changes.

When the performance of a frequency converter is determined, conversion transconductance is used in the same way as transconductance is used in single-frequency amplifier computations.

Deflection Factor of a cathode-ray oscillograph tube is the reciprocal of the deflection sensitivity. 3E11

Deflection Sensitivity of a cathode-ray oscillograph tube is the quotient of the displacement of the electron beam at the place of impact by the change in the deflecting field. It is usually expressed in millimeters per volt applied between the deflecting electrodes or in millimeters per gauss of the deflecting magnetic field.

3E10

Direct Capacitance between two electrodes in a multielectrode tube is the ratio of the charge placed on either electrode to its resulting change in potential above the other electrode when all remaining (n-2) electrodes are at the potential of the first electrode, the charge placed on the second electrode being equal to the sum of the charges placed on all the other electrodes.

Electrode Current is the current passing to or from an electrode through the vacuous space. 1E39

The terms grid current, anode current, plate current, etc., are used to designate currents passing to or from these specific electrodes.

Electrode Dissipation is the power dissipated in the



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form of heat by an electrode as a result of electron and/or ion bombardment. 1E46

Electrode Voltage is the voltage between an electrode and a specified point of the cathode. 1E40

The terms grid voltage, anode voltage, plate voltage, etc., are used to designate the voltage between these specific electrodes and the cathode.

Gas Amplification Factor of a phototube is the factor of increase in the sensitivity of a gas phototube due solely to the ionization of the contained gas. For a gas phototube having a structure such as to permit saturation to occur at a voltage (approximately 25 volts) less than that causing appreciable ionization, the gas amplification factor at a specified operating voltage is the ratio of the sensitivity measured at that voltage to the sensitivity measured at the saturation voltage.

4E5

Grid Driving Power is the average product of the instantaneous value of the grid current and of the alternating component of the grid voltage over a complete cycle. This comprises the power supplied to the biasing device and to the grid.

1E42

Input Capacitance of a vacuum tube is the sum of the direct capacitances between the control grid and the cathode and such other electrodes as are operated at the alternating potential of the cathode. This is not the effective input capacitance, which is a function of the impedances of the associated circuits.

Modulation Factor in an amplitude-modulated wave is the ratio of half the difference between the maximum and minimum amplitudes to the average amplitude.

In linear modulation the average amplitude of the envelope is equal to the amplitude of the unmodulated wave, provided there is no zero-frequency com-





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ponent in the modulating signal wave (as in telephony). For modulating signal waves having unequal positive and negative peaks, positive and negative modulation factors may be defined as the ratios of the maximum departures (positive and negative) of the envelope from its average value to its average value. (See Percentage Modulation.)

1T-39

Mu-Factor ( $\mu$ -factor) is the ratio of the change in one electrode voltage to the change in another electrode voltage, under the conditions that a specified current remains unchanged and that all other electrode voltages are maintained constant. It is a measure of the relative effect of the voltages on two electrodes upon the current in the circuit of any specified electrode. As most precisely used, the term  $\mu$ -factor refers to infinitesimal changes. 1E61

Output Capacitance of a vacuum tube is the sum of the direct capacitances between the output electrode (usually the plate) and the cathode and such other electrodes as are operated at the alternating potential of the cathode. This is not the effective output capacitance, which is a function of the impedances of the associated circuits.

Peak Forward Plate Voltage is the maximum instantaneous plate voltage in the direction in which the tube is designed to pass current. 1E43

Peak Inverse Plate Voltage is the maximum instantaneous plate voltage in the direction opposite to that in which the tube is designed to pass current.

1E44

Peak Plate Current is the maximum instantaneous plate current passing recurrently through the tube in the direction of normal current flow.

Percentage Modulation is the modulation factor expressed in per cent. 1T-40

Plate Resistance is the quotient of the alternating



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plate voltage by the in-phase component of the alternating plate current, all other electrode voltages being maintained constant. This is the effective parallel resistance and is not the real component of the electrode impedance. As most precisely used, the term refers to infinitesimal amplitudes.

Sensitivity of a phototube is basically defined as the quotient of the current through the tube by the radiant flux received by the cathode. The term "radiant flux" includes both visible radiation (light) and invisible infra-red and ultra-violet radiation. When stated in accordance with this basic definition, sensitivity is usually given in terms of microamperes per microwatt of radiant flux.

For convenience, sensitivity is frequently stated in terms of visible radiation only, and is then known as Luminous Sensitivity. When so stated, it is usually expressed in terms of microamperes per lumen of light flux, and depends on the color of the light or the spectral distribution of the radiant flux used to excite the phototube.

2870 Tungsten Sensitivity is the luminous sensitivity when the incident luminous flux is produced by a tungsten-filament lamp at a color temperature of 2870 degrees Kelvin.

When a phototube is used under steady illumination, its luminous sensitivity is known as Static Luminous Sensitivity. This is defined as the direct anode current produced by the light flux divided by the incident light flux of constant value.

When the light input to a phototube varies, as at audio frequency in sound reproduction, the luminous sensitivity is identified as Dynamic Sensitivity, and may be conveniently defined as the quotient of the amplitude of variation in anode current to the amplitude of variation in light input.

In high-vacuum phototubes, the dynamic sensitivity



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is ordinarily independent of frequency. In gas phototubes, the dynamic sensitivity falls off at the higher frequencies because there is a time lag between the current component produced by the secondary electrons resulting from excited atoms and positive ions arriving at the cathode. As the phase difference between these two components increases with increasing frequency of light variation, the net current variation decreases with consequent reduction in sensitivity. In the application of gas phototubes to audio frequencies, this effect is relatively unimportant but can be compensated for, if desired, in the design of the associated amplifier.

In the design of equipment utilizing phototubes, consideration should always be given to the effect of the time constant of the circuit consisting of the phototube and its associated load in reducing the performance capability of the phototube with increasing frequency.

Transconductance from one electrode to another is the quotient of the in-phase component of the alternating current of the second electrode by the alternating voltage of the first electrode, all other electrode voltages being maintained constant. As most precisely used, the term refers to infinitesimal amplitudes.

1E55

Tube Voltage Drop in a gas or vapor-filled tube is the plate voltage during the conducting period.

1E45



#### AND THEIR SIGNIFICANCE

A rating is a designation, as established by definite standards, of an operating limit of a tube. Tubes are rated by either of two systems, i.e., the "absolute maximum" system or the "design-center maximum" system. Of the two, the absolute maximum system is the older and dates back to the beginning of tubes. With either system, each maximum rating for a given tube type must be considered in relation to all other maximum ratings for that type, so that no one maximum rating will be exceeded in utilizing any other maximum rating. For convenience in referring to these two systems, the former will hereinafter be called the "absolute system," and the latter, the "design-center system."

In the absolute system,\* the maximum ratings shown for each type thus rated are limiting values above which the serviceability of the tube may be impaired from the viewpoint of life and satisfactory performance. Therefore, in order not to exceed these absolute ratings, the equipment designer has the responsibility of determining an average design value for each rating below the absolute value of that rating by an amount such that the absolute values will never be exceeded under any usual condition of supply-voltage variation, load variation, or manufacturing variation in the equipment itself.

The equipment should be designed to operate the filament or heater of each tube type at rated normal value for full-load operating conditions under average voltage-supply conditions. Variations from this normal value due to voltage-supply fluctuation or other causes, should not exceed  $\pm 5$  per cent unless otherwise specified by the tube manufacturer.

<sup>\*</sup> Types rated according to the absolute system have no identification on their data pages issued prior to April 1, 1942. Sheets issued after that date carry the statement "Maximum Ratings Are Absolute Values" preceding the ratings.



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In the design-center system\*\* adopted by the receiving-tube industry late in 1939, the maximum ratings shown for each type thus rated are working design-center maximums. The basic purpose underlying this system is to provide satisfactory average performance in the greatest number of equipments on the premise that they will not be adjusted to local power-supply conditions at time of installation. In the setting up of design-center ratings, consideration has been given to three important kinds of power supply commonly in use, i.e., a-c and d-c power lines, storage battery with connected charger, and dry batteries.

In the case of a-c or d-c power lines, the maximum ratings for tubes rated according to the designcenter system have been chosen so that the tubes will give satisfactory performance at these maximum ratings in equipment operated from powerline supplies whose normal voltage including normal variations fall within ±10 per cent of a specified center value. In other words, it is basic to the design-center system of ratings for tubes operated from power-line supplies that filaments or heaters as well as positive- and negative-potential electrodes may have to operate at voltages differing as much as  $\pm 10$  per cent from their rated values. It also recognizes that equipment may occasionally be used on power-line supplies outside the normal range, but since such extreme cases are the exception, they should be handled by adjustment made locally.

The choice of  $\pm 10$  per cent takes care of voltage differences in power lines in the U.S.A. where surveys have shown that the voltages delivered fall within  $\pm 10$  per cent of 117 volts. Therefore, satisfactory performance from tubes rated according to the design-center system will ordinarily be obtained

<sup>\*\*</sup> Types rated according to the design-center system are identified on their data pages either by a large star in the index corner or by the statement "Maximum Ratings Are Design-Center Values" preceding the ratings. This statement is used on sheets issued since April 1, 1942.



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anywhere in the U.S.A. in equipment designed so that the design-center maximum ratings are not exceeded at a line-voltage-center value of 117 volts. While 117 volts represents present-day conditions, the design-center system permits the utilization of a new line-center value as new surveys may indicate the necessity for such a change.

In the case of storage-battery-with-charger supply or similar supplies, the normal battery-voltage fluctuation may be as much as 35 per cent or more. This fluctuation imposes severe operating conditions on tubes. Under these conditions, latitude for operation of tubes is provided for by the stipulation that only 90 per cent of the design-center maximum values of plate voltages, screen-supply voltages, dissipations, and rectifier output currents is never exceeded for a terminal potential at the battery source of 2.2 volts per cell. While a tube's operating voltages in this service will at times exceed the maximum values, satisfactory performance with probable sacrifice in life will be obtained.

In the cases of dry-battery supply and rectified a-c supply for 1.4-volt tubes, recommended design practice is given in RMA Standard M8-210.

RMA Standard M8-210 (Jan. 8, 1940 Rev. 11-40) is reproduced here for the convenient reference of design engineers with permission of the Engineering Department of the Radio Manufacturers Association. Although worded to cover only receiving tubes, it can be applied to any tube having design-center-system ratings.

It shall be standard to interpret the ratings on receiving types of tubes according to the following

conditions:

1. CATHODE—The heater or filament voltage is given as a normal value unless otherwise stated. This means that transformers or resistances in the heater or filament circuit should be designed to op-



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erate the heater or filament at rated value for fullload operating conditions under average supplyvoltage conditions. A reasonable amount of leeway is incorporated in the cathode design so that moderate fluctuations of heater or flament voltage downward will not cause marked falling off in response: also, moderate voltage fluctuations upward will not reduce the life of the cathode to an unsatisfactory degree.

A. 1.4-Volt Battery Tube Types-The filament power supply may be obtained from dry-cell batteries, from storage batteries, or from a power line. With dry-cell battery supply, the filament may be connected either directly across a battery rated at a terminal potential of 1.5 volts, or in series with the filaments of similar tubes across a power supply consisting of dry cells in series. In either case, the voltage across each 1.4-volt section of filament should not exceed 1.6 volts. With power-line or storage-battery supply, the filament may be operated in series with the filaments of similar tubes. For such operation, design adjustments should be made so that, with tubes of rated characteristics, operating with all electrode voltages applied and on a normal line voltage of 117 volts or on a normal storage-battery voltage of 2.0 volts per cell (without a charger) or 2.2 volts per cell (with a charger). the voltage drop across each 1.4-volt section of filament will be maintained within a range of 1.25 to 1.4 volts with a nominal center of 1.3 volts. In order to meet the recommended conditions for operating filaments in series from dry-battery. storage-battery, or power-line sources it may be necessary to use shunting resistors across the individual 1.4-volt sections of filament.

B. 2.0-Volt Battery Tube Types—The 2.0-volt line of tubes is designed to be operated with 2.0 volts across the filament. In all cases the operat-



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ing voltage range should be maintained within the limits of 1.8 volts to 2.2 volts.

- 2. POSITIVE POTENTIAL ELECTRODES The power sources for the operation of radio equipment are subject to variations in their terminal potential. Consequently, the maximum ratings shown on the tube-type data sheets have been established for certain Design Center Voltages which experience has shown to be representative. The Design Center Voltages to be used for the various power supplies together with other rating considerations are as given below:
  - A. AC or DC Power Line Service in U.S.A.—The design center voltage for this type of power supply is 117 volts. The maximum ratings of plate voltages, screen-supply voltages, dissipations, and rectifier output currents are design maximums and should not be exceeded in equipment operated at a line voltage of 117 volts.
  - B. Storage-Battery Service—When storage-battery equipment is operated without a charger, it should be designed so that the published maximum values of plate voltages, screen-supply voltages, dissipations, and rectifier output currents are never exceeded for a terminal potential at the battery source of 2.0 volts per cell. When storage-battery equipment is operated with a charger, it should be designed so that 90% of the same maximum values is never exceeded for a terminal potential at the battery source of 2.2 volts.
  - C. "B"-Battery Service—The design center voltage for "B" batteries is the normal voltage rating of the battery block, such as 45 volts, 90 volts, etc. Equipment should be designed so that under no condition of battery voltage will the plate voltages, the screen-supply voltages, or dissipations ever exceed the recommended respective maximum values shown in the data for each tube type by more than 10%.



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#### D. Other Considerations

- a. Class A<sub>1</sub> Amplifiers—The maximum plate dissipation occurs at the "Zero-Signal" condition. The maximum screen dissipation usually occurs at the condition where the peak-input signal voltage is equal to the bias voltage.
- b. Class B Amplifiers—The maximum plate dissipation theoretically occurs at approximately 63% of the "Maximum-Signal" condition, but practically may occur at any signal voltage value.
- c. Converters—The maximum plate dissipation occurs at the "Zero-Signal" condition and the frequency at which the oscillator-developed bias is a minimum. The screen dissipation for any reasonable variation in signal voltage must never exceed the rated value by more than 10%.
- d. Screen Ratings—When the screen voltage is supplied through a series voltage-dropping resistor, the maximum screen voltage rating may be exceeded, provided the maximum screen dissipation rating is not exceeded at any signal condition, and the maximum screen voltage rating is not exceeded at the maximum-signal condition. Provided these conditions are fulfilled, the screen-supply voltage may be as high as, but not above, the maximum plate voltage rating.
- 3. TYPICAL OPERATION For many receiving tubes, the data show typical operating conditions in particular services. These typical operating values are given to show concisely some guiding information for the use of each type. They are not to be considered as ratings, because the tube can be used under any suitable conditions within its rating limitations.







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#### RECEIVING TUBES

The ratings of all receiving tubes currently used in new equipment are set up according to the design-center system. Older and obsolescent types of receiving tubes still have absolute maximum ratings because these types are used only for renewal purposes and, therefore, design-center values are of no practical value. Receiving-tube types rated on the design-center system are identified in the Receiving-Tube Section either by a large star in the index corner of each data page or by the statement "Maximum Ratings Are Design-Center Values" preceding the ratings on each data page.

#### TRANSMITTING TUBES

The ratings of transmitting tubes grouped in the Transmitting-Tube Section are on the basis of the absolute system. This system enables the transmitter design engineer to choose his design values so as to obtain maximum performance within the tube ratings. Such design procedure has been considered practical for large transmitters where adequate controls are usually incorporated in the design, and ordinarily an experienced operator is present to make any necessary adjustments.

The maximum ratings given for each transmitting type on its data pages apply only when the type is operated at frequencies lower than some specified value which depends on the design of the type. As the frequency is raised above the specified value, the radio-frequency currents, dielectric losses, and heating effects increase rapidly. Most types can be operated above their specified maximum frequency provided the plate voltage and plate input are reduced in accordance with the information given in the table "Transmitting-Tube Ratings vs Operating Frequency" in the front part of the Transmitting-Tube Section.

For certain air-cooled transmitting tubes, two sets



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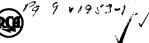
of absolute maximum values are shown to meet diversified design requirements. One set is designated as CCS (Continuous Commercial Service) ratings, while the other is called ICAS (Intermittent Commercial and Amateur Service) ratings.

Continuous Commercial Service is defined as that type of service in which long tube life and reliability of performance under continuous operating conditions are the prime consideration. To meet these requirements, the CCS ratings have been established.

Intermittent Commercial and Amateur Service is defined to include the many applications where the transmitter design factors of minimum size, light weight, and maximum power output are more important than long tube life. These various factors have been taken into account in establishing the ICAS ratings.

Under the ICAS classification are such applications as the use of tubes in amateur transmitters, and the use of tubes in equipment where transmissions are of an intermittent nature. The term "intermittent" is used to identify operating conditions in all applications other than amateur in which no operating or "on" period exceeds 5 minutes and every "on" period is followed by an "off" or standby period of at least the same or greater duration.

ICAS ratings are considerably higher than CCS ratings. They permit the handling of greater power, but tube life under ICAS conditions, of course, is reduced. However, the transmitter designer may very properly decide that a small tube operated with ICAS ratings better meets his requirements than a larger tube operated with CCS ratings. Although such use involves some sacrifice in tube life, the period over which tubes will continue to give satisfactory performance in intermittent service can be extremely long depending on the exact nature of the service.



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The choice of tube operating conditions best fitted for any particular application should be based on a careful consideration of all pertinent factors.

#### RECTIFIER TUBES

Rectifier tubes used principally in receiving equipment are rated according to the design-center system, while those used primarily in transmitting and laboratory equipment are rated according to the absolute system. The method of identifying which rating system is used for any rectifier tube in this Handbook is the same as that for other tubes in the particular section of the Handbook in which data for the rectifier tube are given.

The ratings of rectifier tubes are based on fundamental limitations in the operation of the tubes themselves, and in general include the following: maximum peak inverse plate voltage, maximum peak plate current, and maximum d-c output current.

Maximum peak inverse plate voltage is the highest instantaneous plate voltage which the tube can withstand recurrently in the direction opposite to that in which it is designed to pass current. For mercury-vapor tubes and gas-filled tubes, it is the safe top value to prevent arc-back in the tube operating within the specified temperature range.

In determining peak inverse plate voltage on a rectifier tube in a particular circuit, the equipment designer should remember that the relations between peak value of inverse plate voltage, rms value of input voltage, and average value of output voltage, depend largely on the characteristics of the particular rectifier circuit and the power supply. Furthermore, the presence of transients, such as line surges and keying surges, or waveform distortion, may raise the actual inverse plate voltage to a peak higher than that calculated for sine-wave voltages. Therefore, the actual inverse plate voltage on a rec-

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(continued from preceding page)

tifier tube should never exceed the maximum peak inverse plate voltage rating for that tube. The peak inverse plate voltage may be determined with an electronic peak voltmeter of the self-contained battery type.

In single-phase, full-wave rectifier circuits with sine-wave input and pure resistance lead, the peak inverse plate voltage is approximately 1.4 times the rms value of the plate-to-plate voltage supply. In single-phase, nair-wave circuits with sine-wave input and pure resistance load, the peak inverse plate voltage is approximately 1.4 times the rms value of the plate voltage supply, but with condenser input to fitter, the peak inverse plate voltage may be as high as 2.8 times the rms value of the plate voltage supply.

Maximum peak plate current is the highest instantaneous plate current that a tube can safely carry recurrently in the direction of normal current flow. The safe value of this peak current in hot-cathode types of rectifier tubes is a function of the electron emission available and the duration of the pulsating current flow from the rectifier tube in each half-cycle.

The value of peak plate current in a given rectifier circuit is largely determined by filter constants. If a large choke is used at the filter input, the peak plate current is not much greater than the load current; but if a large condenser is used at the filter input, the peak current may be many times the load current. In order to determine accurately the peak plate current in any rectifier circuit, the designer should measure it with a peak-indicating meter or use an oscillograph.

Maximum d-c output current is the highest average plate current which can be handled continuously by a rectifier tube. Its value for any rectifier tube type is based on the permissible plate dissipation of that type. Under operating conditions involving a rapidly



(continued from preceding page)

repeating duty cycle (steady load), the average plate current may be measured with a d-c meter. In the case of certain mercury-vapor tubes where the load is fluctuating, it is necessary to determine the average current over the time interval specified on the data pages for these types.

In addition to the above ratings for rectifier tubes, other ratings may be set up for a rectifier tube when the service in which the tube is to be used makes such ratings essential for satisfactory performance. Such ratings are: maximum surge plate current, and maximum heater-cathode potential.

Maximum surge plate current is the highest value of abnormal peak currents of short duration that should pass through the rectifier tube under the most adverse conditions of service. This value is intended to assist the equipment designer in a choice of circuit components such that the tube will not be subjected to disastrous currents under abnormal service conditions approximating a short circuit. This surge-current rating is not intended for use under normal operating conditions because subjecting the tube to the maximum surge current even only once may impair tube life. If the tube is subjected to repeated surge currents, its life will be seriously reduced or even terminated.

Maximum heater-cathode potential is the highest instantaneous value of voltage that a rectifier tube can safely stand between its heater and cathode. This rating is applied to certain rectifier tubes having a separate cathode terminal and used in applications where excessive potential may be introduced between heater and cathode. For convenience, this rating is usually given as a d-c value.

# CATHODE-RAY TUBES

The ratings of some cathode-ray tubes are set up on the absolute system while others are set up on the design-center system. Initially, cathode-ray tubes

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(continued from preceding page)

were all rated according to the absolute system. With the advent of television which presented design conditions similar to those in the receiving-set field, the method of rating popular types of cathoderay tubes was changed to the design-center system. More recently, because of procedure standardized by the RMA Cathode-Ray-Tube Committee, newer types of cathode-ray tubes are being rated on the absolute system. Cathode-ray types rated according to the design-center system are identified in the Cathode-Ray Types Section by a statement to that effect just ahead of the maximum ratings on each data page. The data pages of types rated according to the absolute system have either (1) no identifying statement as to the rating system, or (2) an identifying statement that the ratings are according to the absolute system.

#### **PHOTOTUBES**

The ratings of all phototubes in the Phototube Section are on the absolute maximum basis. This basis enables the designing engineer to choose design values so as to obtain optimum performance within tube ratings. In the case of gas phototubes, the value to which the plate voltage and the plate current can be raised is abruptly limited by ionization effects. If these are allowed to occur, they may ruin the photosurface almost instantly. While phototubes in general might be rated on the design-center basis, such a procedure, with provision for an adequate factor of safety to take care of all conditions of operation, would impose undue limitations on the use of gas phototubes.

# MISCELLANEOUS SPECIAL TUBES

The ratings of some of the various tube types grouped in the Miscellaneous-Types Section are according to the design-center system while others are according to the absolute system. Miscellaneous types rated on the design-center basis are identified



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## TUBE RATINGS

(continued from preceding page)

by a statement to that effect on the data pages or else refer back for ratings to a receiving-tube type whose rating basis is explained under TUBE RATINGS—Receiving Tubes. The data pages of types rated according to the absolute system have either (1) no identifying statement as to the rating system, or (2) an identifying statement that the ratings are according to the absolute system.

# CHARACTERISTICS and TYPICAL OPERATING CONDITIONS

In addition to showing the ratings of each tube type, the data pages for many of the types in this Handbook include "characteristics," such as amplification factor, plate resistance, and transconductance, which help to distinguish between the electrical features of the respective types. Usually, the characteristics shown for any type are obtained for that type in class A service: where class A data are given for the type, the characteristics are included with that data for convenience. Based on a large number of tubes of a given type, the values shown for these characteristics are average values.

Range of Characteristics—The equipment designer should bear in mind that individual tubes of a given type may have characteristics values either side of the average values shown for the type. He should also realize that these characteristics change during the life of individual tubes. In designing equipment, therefore, he should allow for the maximum cumulative variation of any characteristic from the average value of that characteristic as shown in the tabulated data for the type. The exact percentage of the variation will be different for different types of tubes depending on the design of the tubes and their intended application, but in general the designer should consider a probable plus or minus variation of not less than 30 per cent.

Furthermore, the equipment designer should recog-



## TUBE RATINGS

(continued from preceding page)

nize the desirability of designing equipment so that the full range of the operating characteristics of tubes will be utilized. If this practice is not followed, he imposes on the equipment user special replacement problems in that the user will have to select tubes suitable for use in the equipment, and may not be able to obtain the full life capability of such tubes.

Typical Operating Values—Also included on the data pages is information on typical operating conditions for most of the various tubes when used in particular services. These typical operating values are intended to show concisely some guiding information for the use of each type. They must not be considered as ratings because each type can, in general, be used under any suitable conditions within its rating limitations. In referring to these values for transmitting tubes, it should be noted that the power output value is not a rating. It is an approximate tube output, i.e., tube input minus plate loss. Circuit losses must be subtracted from tube output in determining useful output.

Datum Point for Electrode Potentials—In the data for any type in the Handbook, the values for grid bias and positive-potential-electrode voltages are given with reference to a specified datum point as follows. For types having filaments heated with d.c., the negative filament terminal is taken as the datum point to which other electrode voltages are referred. For types having filaments heated with a.c., the mid-point (i.e., the center tap on the filament-transformer secondary, or the mid-point on a resistor shunting the filament) is taken as the datum point. For types having equipotential cathodes indirectly heated, the cathode is taken as the datum point.

Grid Bias vs Filament Excitation—If the filament of any type for which data are given on a d-c basis is to be operated with an a-c supply, the given grid



## TUBE RATINGS



(continued from preceding page)

bias should be increased by an amount approximately equal to one half the rated filament voltage and be referred to the filament mid-point. Conversely, if it is required to use d-c filament excitation on any filament type for which the data are given on an a-c basis, the grid-bias values as given on the data pages should be decreased by an amount approximately equal to one half the rated filament voltage and be referred to the negative filament terminal instead of the mid-point as in a-c operation.

In practice, the necessity for following this rule depends on circuit conditions and operating requirements. If the bias is relatively small compared with the filament voltage and hum is a consideration, adjustment of the grid bias is ordinarily essential. Conversely, if the bias is relatively large compared with the filament voltage, adjustment of the grid bias may be unnecessary.

When filament excitation of tubes used as Audio Amplifiers is changed from d.c to a.c., the grid return should, in general, be shifted to the mid-point of the filament circuit to minimize hum, and the bias adjusted accordingly. When the excitation is changed from a.c. to d.c., bias adjustment depending on the relative values of bias and filament voltage may be required to provide the full signal-handling capability of the tubes.

When filament excitation of tubes used as R-F Amplifiers is changed, bias adjustment is not required unless the change makes the circuit critical as to hum or signal-handling capability. For example, in class C amplifiers, the bias is usually so large in comparison with the filament voltage that adjustment is generally unnecessary.

Grid Current and Driving Power—The typical values of d-c grid current and driving power shown for triodes and tetrodes in class B r-f service and in class C service are subject to variations depending on the impedance of the load circuit. High-impe-



## TUBE RATINGS

(continued from preceding page)

dance load circuits require more grid current and driving power to obtain the desired output. Lowimpedance circuits need less grid current and driving power, but plate-circuit efficiency is sacrificed. In comparison, the d-c grid current and driving power shown for beam tubes and pentodes in class B r-f service and in class C service are not as critical to variations in load-circuit conditions. In any event. sufficient grid current should be used so that the stage is "saturated," i.e., so that a small change in grid current results in negligible change in power output. Regardless of the type of tube used, the driving stage should have a tank circuit of good regulation and should be capable of delivering power in excess of the indicated power by a factor of several times.



#### AND THEIR USE

In electron tubes, a cathode is an electrode which is the primary source of electron or ion emission. There are two broad classes of cathodes, i.e., hot and cold. "Hot cathodes" are defined as cathodes which are heated or otherwise operate at elevated temperature (frequently incandescent) in order to function as emitters. In contrast, "cold cathodes" are defined as cathodes which do not rely on heat or on elevated temperature in order to function as emitters.

#### HOT CATHODES

Hot cathodes commonly in use in electron tubes are classified as directly heated, indirectly heated, and ionic-heated.

A directly heated cathode, or filament-cathode, is a wire or ribbon which is heated by the passage of current through it. It is further classified by identifying the filament material or the electron-emitting material. Such materials in regular use are pure tungsten, thoriated tungsten, and metals coated with alkaline-earth oxides. Each of these materials has distinctive advantages which are utilized in the design of tubes for particular applications.

PURE-TUNGSTEN FILAMENTS are used in certain tubes, especially those for high-voltage transmitting service. Since these filaments must operate at a high temperature of about 2500°C (a dazzling white) to emit sufficient electrons, a relatively large amount of filament power is required. The operating life of these filaments is determined by the rate of tungsten evaporation. Their failure, therefore, occurs through decreased emission or burn-out.

Pure-tungsten filaments give best life performance when they are operated so as to conserve their emitting capability. They are designed with voltage and current ratings in accord with the service expected of the particular tube type. However, in applications where the normal emission at rated voltage is not



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required, the filament can be operated at a somewhat reduced voltage. The extent of the reduction depends on the peak emission requirements of the application as well as on the percentage regulation of the filament voltage. When these are known, the correct operating filament voltage for any tungstenfilament type can be calculated from its filamentemission characteristic. The permissible regulation in transmitters may be checked by reducing the filament voltage (with the transmitter under normal operation) to a value such that reduction in output can just be detected. The filament voltage must then be increased by an amount equivalent to the maximum percentage regulation of the filament-supply voltage and then increased further by approximately 2 per cent to allow for minor variations in emission of individual tubes. It follows that the better the regulation, the less the filament operating voltage and, therefore, the longer the filament life.

It should be noted that a reduction of 5 per cent in the filament voltage applied to tubes with pure-tungsten filaments will approximately double their life. A reduction of 15 per cent will increase the filament life almost tenfold.

During long or frequent standby periods, pure-tungsten-filament tubes may be operated at decreased filament voltage to conserve life. When the average standby time is an appreciable portion of the average duty cycle and is less than 2 hours, it is recommended that the filament voltage of all but the largest types be reduced to 80 per cent of normal; and that for longer periods, the filament power be turned off. For the largest types, such as the 898, it is recommended that the filament voltage be reduced to 80 per cent of normal during standby operation up to 12 hours; and that for longer periods, the filament power be turned off.

For turning on filament power, a filament starter should be used so as to increase the voltage gradually and to limit the high initial rush of current through





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the filament. It is important that the filament current never exceed, even momentarily, a value of more than 150 per cent of normal, unless the tube data specify otherwise. Similarly, as an added precaution, the filament power should be turned off gradually to prevent cooling strains in the filament.

THORIATED-TUNGSTEN FILAMENTS are now used mainly in certain transmitting and special tubes. Thoriated-tungsten filaments are made from tungsten impregnated with thoria. Due to the presence of thorium, these filaments liberate electrons at a more moderate temperature of about 1700°C (a bright yellow), and are, therefore, much more economical of filament power than are pure-tungsten filaments. The operating life of thoriated-tungsten filaments is ordinarily ended by a decrease in electron emission. Decreased emission, however, may be caused by the accidental application of too high filament, screen, or plate voltage. If the over-voltage has not been continued for a long time, the activity of the filament can often be restored by operating the filament at its normal voltage for 10 minutes or longer without plate, screen, or grid voltage. The reactivation process may be accelerated by raising the filament voltage to not higher than 120 per cent of normal value for a few minutes. This reactivation schedule is often effective in restoring the emission of thoriated-tungsten filaments in tubes which have failed after normal service. Sometimes a few hundred hours of additional life may be obtained after reactivation.

The operating voltage of a thoriated-tungsten filament should, in general, be held to within  $\pm 5$  per cent of its rated value. However, in transmitting applications where the tube is lightly loaded, the filament may be operated on the low side—as much as 5 per cent below normal voltage. As conditions require, the voltage should be increased gradually to maintain output. Toward the end of life, additional service may be obtained by operating the fila-



(continued from preceding page)

ment above its rated voltage. It should be noted that a tube having a thoriated-tungsten filament should never be operated under emission-limited conditions since this type of operation may overheat the tube and cause permanent loss of emission.

During standby periods in transmitting service, thoriated-tungsten filaments may be operated according to the following recommendations to conserve life. For short standbys of less than 15 minutes duration, the filament voltage of all but the largest types should be reduced to 80 per cent of normal; for longer periods, the filament power should be turned off. For the largest types, such as the 827-R and 861, it is recommended that the filament voltage be reduced to 80 per cent of normal during standby operation up to 2 hours; and that for longer periods, the filament power be turned off.

COATED FILAMENTS are used in receiving tubes, certain transmitting tubes, most mercury-vapor rectifiers, and some special tubes. Coated filaments employ a relatively thick coating of alkaline-earth compounds on a metallic base as a source of electronic emission. The metallic base carries the heating current. These filaments operate at a low temperature of about 800°C (a dull red) and require relatively little power to produce a copious supply of electrons.

For proper performance of these types, rated filament voltage should, in general, be applied at the filament terminals. However, when coated-filament, high-vacuum tubes are used in transmitting service with light loading, the filament voltage may be reduced as much as 5 per cent below normal to conserve life. Then, as conditions require, the voltage should be increased gradually to maintain output. Toward the end of life, the gradual increase may be carried above rated filament voltage to obtain additional service. In the case of gas or vapor tubes, it is important that these types be operated, in general, at rated filament voltage. However, if the line regu-



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lation regularly and consistently does not exceed 1 to 2 per cent, it is practical to reduce the filament voltage slightly (not over 5 per cent) with benefit to tube life.

During standby periods of less than 15 minutes, the filament voltage of quick-heating, high-vacuum types, such as the 1616 and 1624, should be reduced to 80 per cent of normal; for longer periods, the filament power should be turned off. In contrast, the voltage of coated filaments in gas or vapor tubes should not be reduced during standbys except under conditions explained in the preceding paragraph. In general, the filament voltage of small and medium types, such as the 866-A/866 and 872-A/872, should be maintained at normal rated value during standbys up to 2 hours; for longer periods, the filament power should be turned off. For large types. such as the 857-B, the filament voltage should be maintained at normal rated value during standbys up to 12 hours; for longer periods, the filament power should be turned off.

After having given normal service or after having been operated at excessive voltage, coated filaments lose their emission. When such is the case, their usefulness may be considered as terminated.

An indirectly heated cathode, or heater-cathode, consists of a heater wire enclosed in a thin metal sleeve coated on the outside with electron-emitting material similar to that used for coated filaments. The sleeve is heated by radiation and conduction from the heater through which current is passed. Useful emission does not take place from the heater wire. An important feature of this kind of cathode construction is that the functions of heating and emission can be independent of each other.

HEATER-CATHODES, or unipotential cathodes as they are frequently called, are used in high-vacuum tubes operating at low plate voltage, such as receiv-



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ing tubes, low-power transmitting tubes, and small special tubes. They also find application in mercury-vapor tubes and in cathode-ray tubes. Heater-cathodes, like coated filaments, provide a copious supply of electron emission at low cathode temperature (a dull red).

For proper performance of heater-cathode tubes, rated heater voltage should, in general, be applied at the heater terminals. However, when heater-cathode high-vacuum tubes are used in transmitting service and are lightly loaded, the heater voltage may be reduced as much as 5 per cent below normal to conserve life. As conditions require, the voltage should be increased gradually to maintain output. Toward the end of life, the gradual increase may be carried above rated heater voltage to obtain additional service.

During standby periods of less than 15 minutes, the heater voltage of high-vacuum tubes should be maintained at normal rated value; for longer periods, the heater power should be turned off. In the case of vapor or gas tubes, the heater voltage should be maintained at normal during standby periods up to 12 hours; for longer periods, the heater power should be turned off.

An ionic-heated cathode is one which liberates electrons when it is subjected to intense positive ion bombardment. The bombardment may be so intense as to raise the temperature of the cathode, frequently causing it to become visibly hot. The ionic-heated cathode in radio tubes has found application in gas rectifiers intended primarily for automobile receiver service.

#### COLD CATHODES

The designation "cold cathode" is commonly used in referring to those cathodes which emit electrons when they are subjected to bombardment by other electrons, ions, or metastable atoms. Cathodes of



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this type are sometimes designated as secondaryemission cathodes. They are used in certain glowdischarge tubes, and also in multiplier phototubes where they contribute to electron multiplication in the successive dynode stages.

Not customarily referred to as cold cathodes, although they are such, is another group of emitters known as photocathodes. By definition, a photocathode is one which emits electrons when it is energized with radiant flux, such as light, infra-red radiation, or ultra-violet radiation. Such cathodes are used in phototubes. When used in gas phototubes, these cathodes not only emit under the influence of radiant flux but also as a result of bombardment and thus become partial secondary-emission cathodes.

Photocathodes are classified according to the spectral response characteristics of their respective photoactive surfaces. The S1 photosurface gives high response to red and near infra-red radiation. The S2 photosurface is similar to the S1 surface but extends somewhat further into the infra-red region. The S3 photosurface has a spectral response characteristic which is closest to that of the eye. The S4 photosurface has exceptionally high response to blue and blue-green radiation with negligible response to red radiation.

Exposure of photocathodes to intense light, such as direct sunlight, may decrease the sensitivity of the tubes in which they are used, even though there is no voltage applied. The magnitude and duration of the decrease depend on the length of the exposure. Permanent damage to a phototube may result if it is exposed to radiant energy so intense as to cause excessive heating of the cathode.





#### CONVERSION FACTORS

FOR POWER AMPLIFIER TRIODES AND PENTODES
These curves are especially useful for calculating

especially These curves are with fair accuracy from published operating conditions, operating conditions to meet other special voltage requirements. plate łΩ To use these curves: First, determine the ratio of the new plate voltage to the published plate voltage est the desired new conditions. This the Voltage Conversion Factor is then used to determine the screen and the new control-grid deteralso used to mine from the curves, factors for the other new operating conditions. FACTORS FL, Fp, Fr, Fgm CONVERSION 0.6 APPLIES TO SCREEN VOLTAGE, TROL-GRID VOLTAGE, AND VOLTAGE APPLIES TO PLATE CURRENT AND TO 0.2 SCREEN CURRENT APPLIES TO POWER OUTPUT APPLIES TO LOAD RESISTANCE TO PLATE RESISTANCE APPLIES TO MUTUAL CONDUCTANCE VOLTAGE CONVERSION FACTOR (Fe)



METAL TUBES Fey to Tube Types

#### OUTLINES VS TUBE TYPES

MT8B			- MT86				MT86 with Miniature Cap	
5W4	6٧6	25Z6	6AB7	65F7	6557	12SH7	6K8	
5Z4	6X5	1611	6AC7	65G7	6S.T7	12SJ7	6 <b>S</b> 7	
6AG7	12A6	1613	605	6SH7	12SA7	125K7	12K8	
6F6	25A6	1621	6.15	6SJ7	12807	12507		
6N7	25L6	1632	6SA7	6SK7	12SF5	12SR7	1	
			6SC7	6507	12SF7	1634	ł	
			6SF5	6SR7	125G7		1	

MT8G with Pin Cap	MT8K	MTTSA	MTTSA with Miniature Cap		MTIOA	
1851	6H6 I 2H6	024	6A8 6B8 6F5 6J7 6K7 6L7	6Q7 6R7 12C8 1612 1620	5T4 6L6 913 1614	1619 1622 1631

#### TUBE TYPES VS OUTLINES

TOBE TIPES VS COTETALS						
Type	Outline	Туре	Outline	Type	Outline	
0Z4	MTT8A	657	MT8G (c)	12SF7	MTBG	
5T4	MTIOA	6SA7	MT8G	12SG7	MT8G	
5W4	MT8B	6SC7	MT8G	12SH7	MT8G	
5Z4	MT8B	6SF5	MT8G	12SJ7	MT8G	
6A8	MTT8A (c)	6SF7	MT8G	12SK7	MT8G	
6AB7	MT8G	6SG7	MT8G	12507	MTBG	
6AC7	MT8G	6SH7	MT8G	12SR7	MTBG	
6AG7	MT8B	6SJ7	MT8G	25A6	MT8B	
688	MTT8A (c)	6SK7	MT8G	25L6	MT8B	
605	MT8G	6SQ7	MT8G	25Z6	MT8B	
6F5	MTT8A (c)	6SR7	MT8G	913	MTIOA	
6F6	MT8B	6557	MT8G	1611	MT8B	
6H6	MTBK	6ST7	- MTBG	1612	MTTBA (c)	
615	MT8G	676	мтвв	1613	MT8B	
6J7	MTT8A (c)	6X5	мтвв	1614	MTIOA	
6K7	MTTBA (c)	12A6	MT8B	1619	MTIOA	
6K8	MT8G (c)	1208	MTT8A (c)	1620	MTTBA (c)	
6L6	MT10A	12H6	мтвк	1621	мтав	
6L7	MTT8A (c)	12K8	MT8G (c)	1622	MTIOA .	
6N7	MT88	12SA7	MT8G	1631	MTIOA	
607	MTTBA (c)	12SC7	MT8G	1632	MT8B	
6R7	MTT8A (c)	12SF5	MT8G	1634	MTBG	
		(c) =	Miniature Cap Pin Cap	1851	MT8G (pc)	

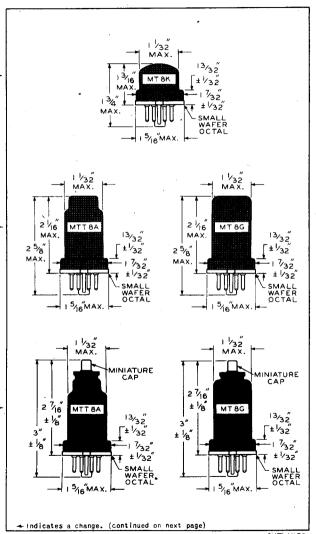
JAN. 15, 1944

RCA VICTOR DIVISION "

METAL TUBE OUTLINES-KEY

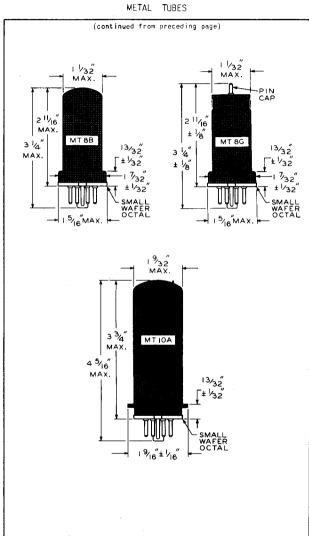


METAL TUBES



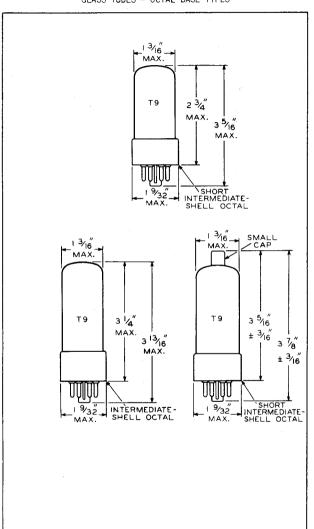








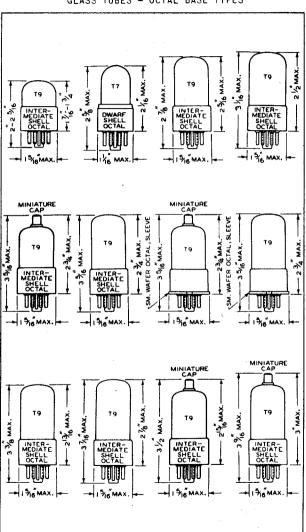
GLASS TUBES - OCTAL BASE TYPES





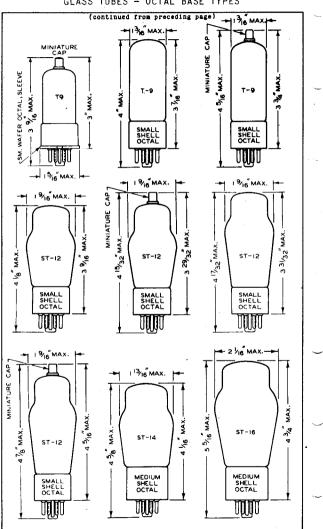


#### GLASS TUBES - OCTAL BASE TYPES



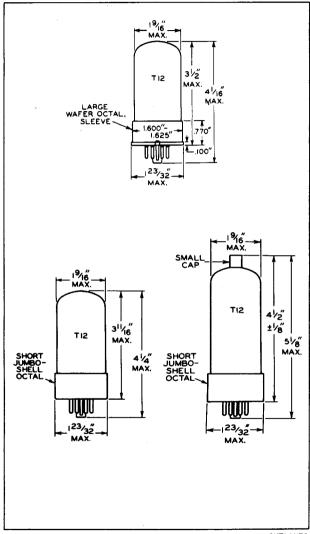


GLASS TUBES - OCTAL BASE TYPES





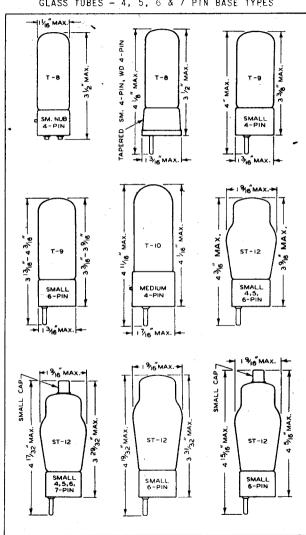
OCTAL BASE TYPES WITH T-12 BULBS





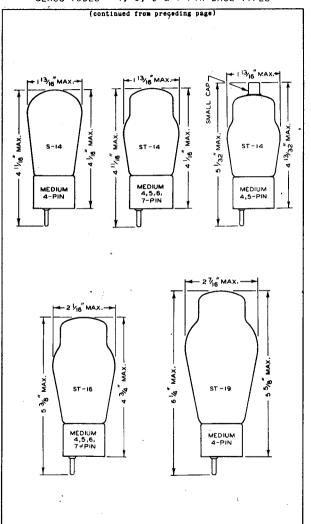


GLASS TUBES - 4, 5, 6 & 7 PIN BASE TYPES





GLASS TUBES - 4, 5, 6 & 7 PIN BASE TYPES

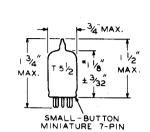


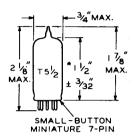


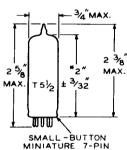


SMALL-BUTTON MINIATURE & NOVAL BASE TYPES

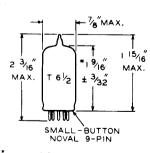
#### SMALL-BUTTON MINIATURE 7-PIN TYPES

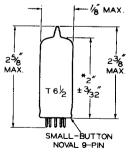






#### SMALL-BUTTON NOVAL 9-PIN TYPES





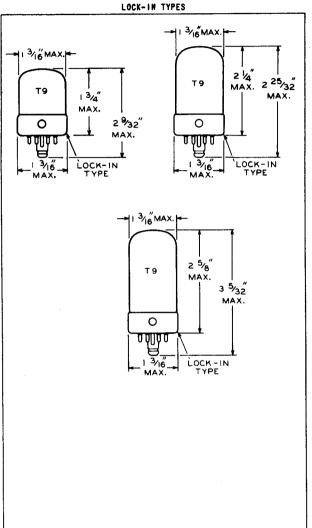
\* Measured from base seat to bulb-top line as determined by ring gauge of 7/16\* I.D.

SEPT. 30, 1948

TUBE DEPARTMENT

OUTLINES

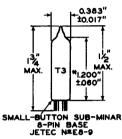




SEPT. 30, 1948



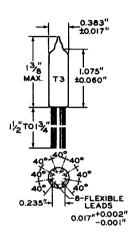
#### SMALL-BUTTON SUB-MINAR BASE TYPE



MEASURED FROM BASE SEAT TO BULB-TOP LINE AS DETERMINED BY A RING GAUGE OF . 210" 1.D.

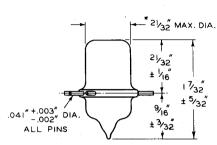


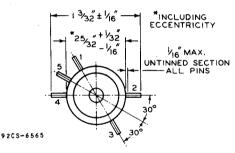
#### FLEXIBLE-LEAD TYPE





RADIAL 5-PIN BASE TYPE





#### BOTTOM VIEW

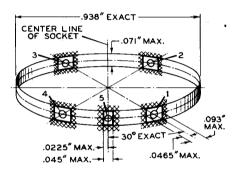
SEE DIAGRAM "A" ON NEXT PAGE FOR ADDITIONAL SOCKET-DESIGN INFORMATION



RADIAL 5-PIN BASE TYPE

#### MAXIMUM PIN VARIATIONS AT SOCKET CLIPS

ESSENTIAL DIMENSIONS FOR SOCKET DESIGN



Nº 1-5 SHOW THE IDEAL POSITIONS OF PIN CROSS-SECTIONS AT SOCKET CLIPS LOCATED ON A CIRCLE OF 0.938" DIAMETER. THE AREAS WITHIN THE CROSS-HATCHING SHOW ACTUAL VARIATIONS OF PIN CROSS-SECTIONS AND INDICATE THE MAXIMUM VARIATIONS WHICH SOCKET CLIPS SHOULD ACCOMODATE FOR THE CIRCLE SHOWN.

THE CLEAR AREA FOR PIN POSITION Nº5 IS NARROWER THAN THE OTHERS BECAUSE PIN Nº5 IS USED AS A REFERENCE FOR OTHER PINS.

SOCKETS SHOULD BE DESIGNED SO THAT THE MINIMUM DIAMETRIC CLEARANCE BETWEEN SOCKET CLIPS IS NEVER LESS THAN 0.850".

#### DIAGRAM A

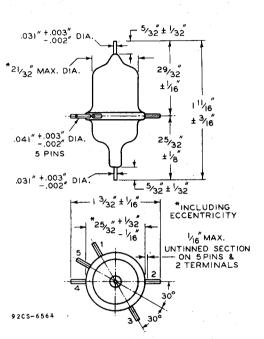
92CM-6563RI



# $\sqrt{\phantom{a}}$

## OUTLINES-Glass Tubes

#### RADIAL 5-PIN BASE TYPE WITH END TERMINALS



#### BOTTOM VIEW

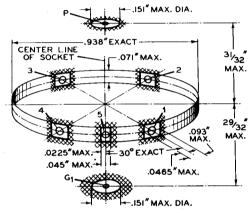
SEE DIAGRAM "B" ON NEXT PAGE FOR ADDITIONAL SOCKET-DESIGN INFORMATION



RADIAL 5-PIN BASE TYPE WITH END TERMINALS

# MAXIMUM PIN AND TERMINAL VARIATIONS AT SOCKET CLIPS AND TERMINAL CONNECTORS

ESSENTIAL DIMENSIONS FOR SOCKET DESIGN



Nº 1-5 SHOW THE IDEAL POSITIONS OF PIN CROSS-SECTIONS AT SOCKET CLIPS LOCATED ON A CIRCLE OF 0.938" DIAMETER. THE AREAS WITHIN THE CROSS-HATCHING SHOW ACTUAL VARIATIONS OF PIN CROSS-SECTIONS AND INDICATE THE MAXIMUM VARIATIONS WHICH SOCKET CLIPS SHOULD ACCOMODATE FOR THE CIRCLE SHOWN.

THE CLEAR AREA FOR PIN POSITION Nº 5 IS NARROWER THAN THE OTHERS BECAUSE PIN Nº 5 IS USED AS A REFERENCE FOR OTHER PINS.

SOCKETS SHOULD BE DESIGNED SO THAT THE MINIMUM DIAMETRIC CLEARANCE BETWEEN SOCKET CLIPS IS NEVER LESS THAN 0.850".

P & G<sub>1</sub> SHOW THE IDEAL POSITIONS OF TERMINAL CROSS-SECTIONS AT TERMINAL ENDS. THE AREAS WITHIN THE CROSS-HATCHING SHOW ACTUAL VARIATIONS OF TERMINAL CROSS-SECTIONS AND INDICATE THE MAXIMUM VARIATIONS WHICH TERMINAL CONNECTORS SHOULD ACCOMODATE.

DIAGRAM B

92CM-6562RI

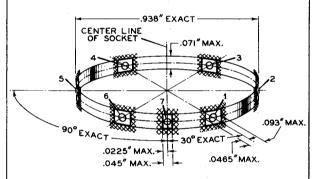
- Indicates a change.



RADIAL 7-PIN BASE TYPE

#### MAXIMUM PIN VARIATIONS AT SOCKET CLIPS

ESSENTIAL DIMENSIONS FOR SOCKET DESIGN



 $N\mathfrak{D}$  1-7 show the IDEAL POSITIONS OF PIN CROSS-SECTIONS AT SOCKET CLIPS LOCATED ON A CIRCLE OF 0.938" DIAMETER. THE AREAS WITHIN THE CROSS-HATCHING SHOW ACTUAL VARIATIONS OF PIN CROSS-SECTIONS AND INDICATE THE MAXIMUM VARIATIONS WHICH SOCKET CLIPS SHOULD ACCOMODATE FOR THE CIRCLE SHOWN.

THE CLEAR AREA FOR PIN POSITION № 7 IS NARROWER THAN THE OTHERS BECAUSE PIN № 7 IS USED AS A REFERENCE FOR OTHER PINS.

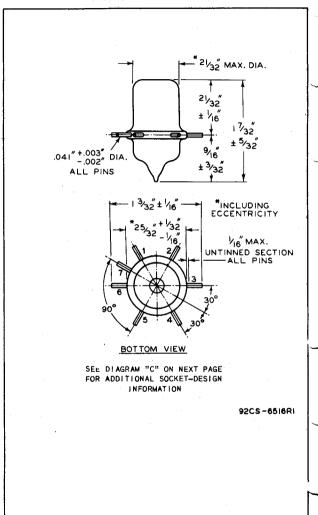
SOCKETS SHOULD BE DESIGNED SO THAT THE MINIMUM DIAMETRIC CLEARANCE BETWEEN SOCKET CLIPS IS NEVER LESS THAN 0.850".

#### DIAGRAM C

92CM-6566



RADIAL 7-PIN BASE TYPE



AUG. 15, 1944

OUTLINES



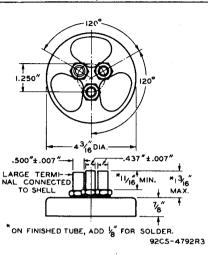
#### MINIMUM DIAMETERS

Until such time as the Handbook pages covering bases are reissued to include minimum diameters of wafers, shells, and sleeves, this provisional sheet will supply these minimum diameters for the following bases to supplement the maximum diameters which are shown on the respective base drawings.

Base	Minimum Diameter
3-PIN & 4-PIN TYPES:	Diameter
Peewee 3-Pin. Small 4-Nub. WD 4-Pin. Tapered Small 4-Pin. Small 4-Pin. Medium 4-Pin. Medium 4-Pin with Bayonet. Jumbo 4-Pin. Super-Jumbo 4-Pin.	0.610" 0.970" 1.097" 1.136" 1.136" 1.337" 1.337" 1.840" 2.177"
5-PIN TYPES:	
Small 5-Pin	1.136" 1.337" 2.142"
6-PIN TYPES:	
Small 6-Pin Medium 6-Pin	1.136" 1.337"
7-PIN TYPES:	
Small 7-Pin	1.337"
8-PIN TYPES:	
Dwarf Shell Octal 8-Pin Dwarf Metal Shell Octal 8-Pin Small Shell Octal 8-Pin Intermediate Shell Octal 8-Pin Small Wafer Octal 8-Pin	1.015" 1.136" 1.235" 1.271"
with Sleeve No. R1483\{\text{Wafer} \text{Sleeve} \text{Sleeve}	1.271" 1.198"
with Sleeve No. T254	1.271" 2.369" 1.337" 1.677"
with Sleeve No. T253	1.677" 1.845"
12-PIN & 14-PIN TYPES:  Medium Shell Diheptal 14-Pin	



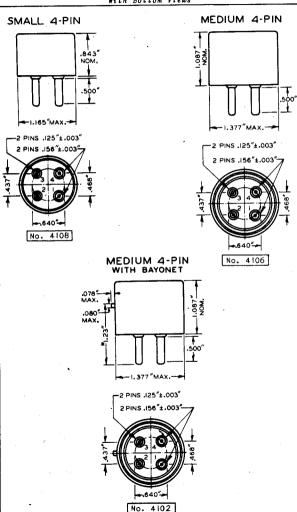
3-TERMINAL TYPES
With Top View



JETEC No.A3-80 RCA No.3232

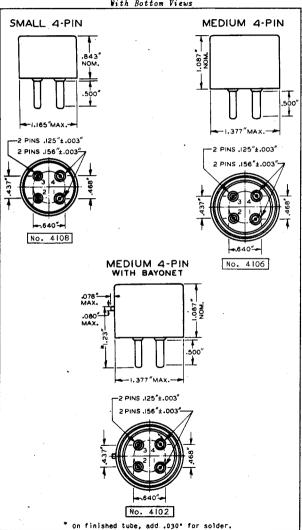


4-PIN TYPES With Bottom Views





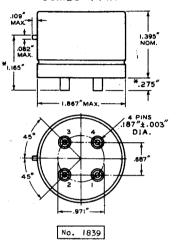
4-PIN TYPES
With Bottom Views





4-PIN TYPES With Bottom View

### JUMBO 4-PIN

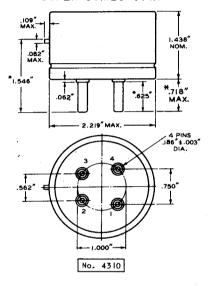


\* On finished tube, add .060" for solder.



4-PIN TYPES With Bottom View

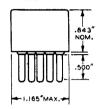
#### SUPER-JUMBO 4-PIN

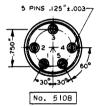


On finished tube, add .030° for solder.

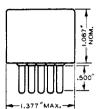


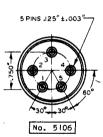
# SMALL 5-PIN





# MEDIUM 5-PIN





DWARF SHELL OCTAL 5-PIN
INTERMEDIATE SHELL OCTAL 5-PIN
MEDIUM SHELL OCTAL 5-PIN
SMALL SHELL OCTAL 5-PIN
SMALL WAFER OCTAL 5-PIN

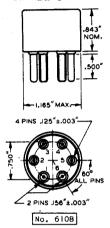
For details of above bases, see corresponding OCTAL 8-PIN type.



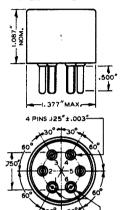
# GIANT 5-PIN 1.750 NOM. "ı.546" 5-PINS .187"±.003" DIA. 1.250 30 No. 5325







### MEDIUM 6-PIN



2 PINS .156"±.003

LONG-SHELL MEDIUM 6-PIN Same As Medium 6-Pin Above, Except That Shell Length is 1.315" Nominal -No. 6105-

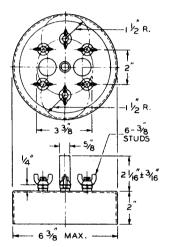
INTERMEDIATE SHELL OCTAL 6-PIN SMALL SHELL OCTAL 6-PIN SMALL WAFER OCTAL 6-PIN SMALL WAFER OCTAL 6-PIN, WITH SLEEVE

For details of above bases, see corresponding OCTAL 8-PIN type.



6-TERMINAL TYPES With Bottom View

# Nº 6628 BASE

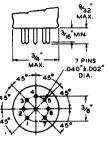


SPACE FOR CONNECTOR BETWEEN WING NUT AND LOCK NUT IS  $\frac{3}{16}$  MAX.

92CM-4438R2



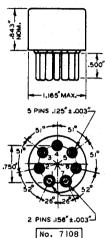
# MINIATURE BUTTON 7-PIN



Sockets for the Miniature Button 7-Pin Base should have a center hole (0.156° min. diameter) extending through the socket. Sockets for ref tube types having this base should have a cylindrical metal sleeve to shield the grid pin from the plate pin. This sleeve should have a minimum inside diameter of 0.135°, and should be long enough to shield opposite socket terminals one from another.

The socket design should be such that circuit wiring cannot impress lateral scrains through the socket contacts on the base pins. The point of bearing of the contacts on the base pins should not be closer than 1/8" from the bottom of a seated tube.

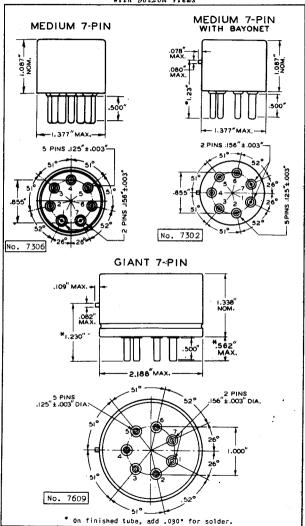
# SMALL 7-PIN



INTERMEDIATE SHELL OCTAL 7-PIN
MEDIUM SHELL OCTAL 7-PIN
SMALL SHELL OCTAL 7-PIN
SMALL WAFER OCTAL 7-PIN
SMALL WAFER OCTAL 7-PIN, WITH SLEEVE

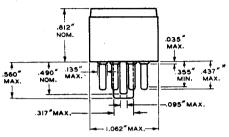
For details of above bases, see corresponding OCTAL 8-PIN type.

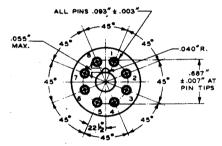






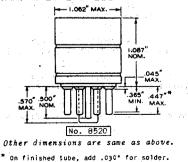
# DWARE SHELL OCTAL 8-PIN





DWARF SHELL OCTAL 5-PIN As Above, Omitting Pins No. 2, 4& 6

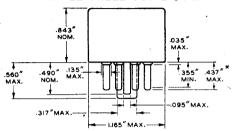
### METAL SHELL OCTAL 8-PIN DWARF

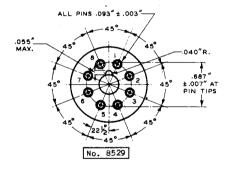


Dec. 1, 1942



# SMALL SHELL OCTAL 8-PIN





SMALL SHELL OCTAL 7-PIN As Above, Omitting Pin No. 6 -No. 7529-

SMALL SHELL OCTAL 6-PIN As Above, Omitting Pins No. 4 & 6 -No. 6529-

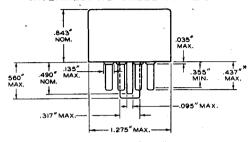
SMALL SHELL OCTAL 5-PIN
Arrangement A - As Above, Omitting Pins No. 3,5 & 6
-No. 5429-

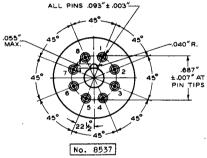
Arrangement B - As Above, Omitting Pins No. 3, 5 & 7
-No. 5529-

\*. On finished tube, add .030\* for solder.



# INTERMEDIATE SHELL OCTAL 8-PIN





INTERMEDIATE SHELL OCTAL 7-PIN As Above, Omitting Pin No. 6 -No. 75374

INTERMEDIATE SHELL OCTAL 6-PIN As Above, Omitting Pins No. 4&6 -No. 6537-

INTERMEDIATE SHELL OCTAL 5-PIN Arrangement A - As Above, Omitting Pins No. 3, 5 & 6 -No. 5437-

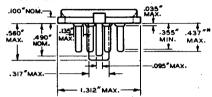
Arrangement B - As Above, Omitting Pins No. 3, 5 & 7

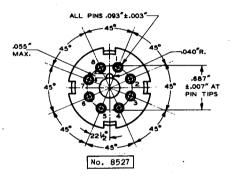
-No. 5537-

\* On finished tube, add .030\* for solder.



# SMALL WAFER OCTAL 8-PIN





SMALL WAFER OCTAL 7-PIN As Above, Omitting Pin No. 6 -No. 7527-

SMALL WAFER OCTAL 6-PIN As Above, Omitting Pins No. 4 & 6 - No. 6527-

SMALL WAFER OCTAL 5-PIN Arrangement A - As Above, Omitting Pins No. 3, 5 & 6 - No. 5427-

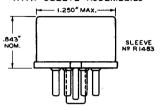
Arrangement B - As Above, Omitting Pins No. 3, 5 & 7
-No. 5527-

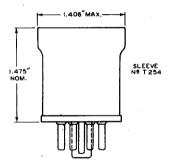
\* on finished tube, add .030" for solder.





# SMALL WAFER OCTAL 8-PIN WITH SLEEVE ASSEMBLIES





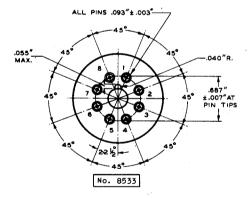
Other dimensions are same as for SMALL WAFER OCTAL 8-PIN BASE

SMALL WAFER OCTAL 7-PIN, WITH SLEEVE As above with Sleeve No. R1483, Omitting Pin No. 6

SMALL WAFER OCTAL 6-PIN, WITH SLEEVE As Above With Sleeve No. R1483, Omitting Pins No. 4 & 6



# MEDIUM SHELL OCTAL 8-PIN 1.087" NOM. .560" 490" MAX. .355" .337" MIN. MAX. .317"MAX. .317"MAX.



MEDIUM SHELL OCTAL 7-PIN As Above, Omitting Pin No. 6

- No. 7533-

MEDIUM SHELL OCTAL 6-PIN As Above, Omitting Pins No. 4& 6

\_-No. 6533-

MEDIUM SHELL OCTAL 5-PIN As Above, Omitting Pins No. 3, 5 & 7

\_ No. 5533-

\* On finished tube, add .030" for solder.



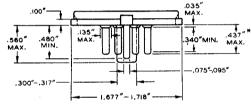
# BASES

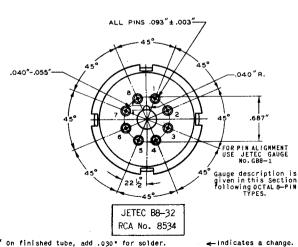
8-PIN TYPES
With Bottom View

LONG MEDIUM-SHELL OCTAL 8-PIN
Same As Medium-Shell Octal 8-Pin On Preceding Page,
Except That Shell Length Is 1.375"

RCA No. 8545

# LARGE-WAFER OCTAL 8-PIN





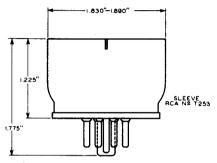
NOV. 1, 1950

TUBE DEPARTMENT

BASES

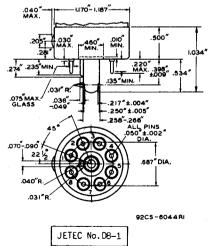


# LARGE-WAFER OCTAL 8-PIN



Other dimensions are same as for LARGE-WAFER OCTAL 8-PIN BASE

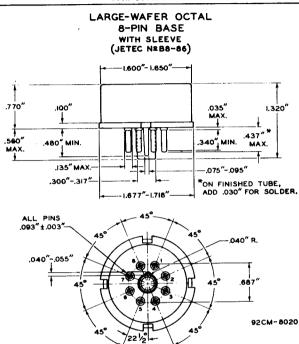
# LOCK-IN 8-PIN



BASES

-> Indicates a change.



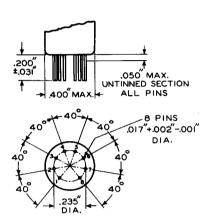


Base-pin positions are held to tolerances such that entire length of pins will enter flat-plate gauge (JETEC No.GB8-1) having thickness of I/4" and eight 0.1030"  $\pm$  0.0005" holes so located on a 0.6870"  $\pm$  0.0005" diameter circle that the distance along the chord between any two adjacent hole centers is 0.2630"  $\pm$  0.0005".

Pin fit in gauge shall be such that gauge together with supplementary weight totaling 2 lbs. will not be lifted when pins are withdrawn.



# SMALL-BUTTON SUB-MINAR 8-PIN BASE

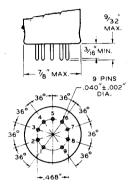


92CS-7158

The design of the socket should be such that the point of bearing of the contacts on the base pins should not be closer than 0.050" from the bottom of the seated tube.



### SMALL-BUTTON NOVAL 9-PIN BASE JETEC Nº E9-I



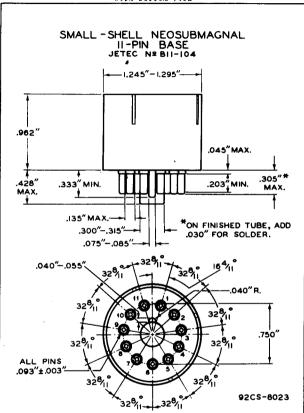
92CS-6694

The pins will fit a flat-plate gauge having thickness of 1/4" and ten holes 0.0520"  $\pm 0.0005$ " so located on a 0.4680"  $\pm 0.0005$ " diameter circle that the distance along the chord between any two adjacent hole centers is 0.1446"  $\pm 0.0005$ ".

The design of socket should be such that circuit wiring can not impress lateral strains through the socket contacts on the base pins. The point of bearing of the contacts on the base pins should not be closer than 1/8" from the bottom of the seated tube.



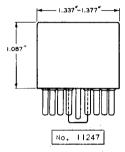
### With Bottom View



Base-pin positions are held to tolerances such that pins will fit flat-plate gauge having thickness of I/4 inch and eleven 0.1030"-0.1035" holes so located on a 0.7500" ± 0.0005" diameter circle that the distance along the chord between any two adjacent hole centers is 0.2125" ± 0.0005". Pin fit in gauge shall be such that entire length of pins will enter gauge, and on withdrawal, they will become disengaged without lifting gauge and supplementary weight totaling 3 pounds.



# SMALL SHELL MAGNAL II-PIN

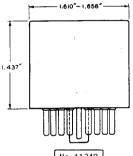


Other dimensions are same as for LARGE WAFER MAGNAL 11-PIN

Indicates a change.



# MEDIUM SHELL MAGNAL II-PIN

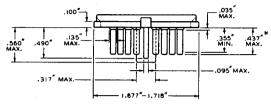


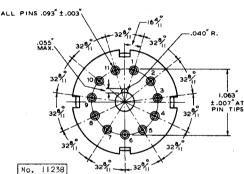
No.11248

Other dimensions are same as shown for LARGE WAFER MAGNAL 11-PIN BASE

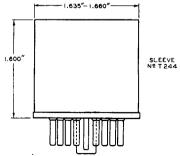


# LARGE WAFER MAGNAL II-PIN





# LARGE WAFER MAGNAL II-PIN WITH SLEEVE ASSEMBLIES



Other dimensions are same as above.

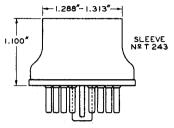
\* On finished tube, add .030" for solder. —— Indicates a change.

DEC. 15. 1944

BASES

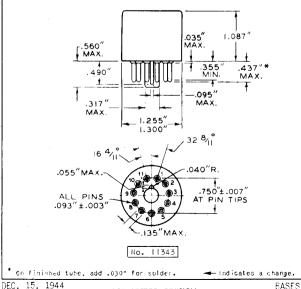


# LARGE WAFER MAGNAL II-PIN WITH SLEEVE ASSEMBLIES (CONT'D)



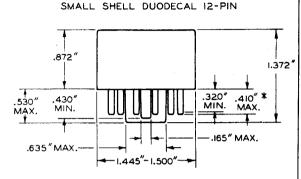
Other dimensions are same as shown on preceding page.

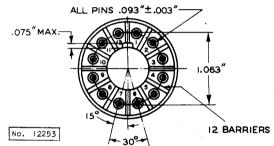
# SMALL SHELL SUBMAGNAL 11-PIN





# With Bottom View





Base-pin positions are held to tolerances such that pins will fit flat-plate gauge having thickness of  $0.25^{\circ}$  and twelve  $0.1030^{\circ}\pm0.0005^{\circ}$  holes so located on a  $1.0630^{\circ}\pm0.0005^{\circ}$  diameter circle that the distance along the chord between any two adjacent hole centers is  $0.2772^{\circ}\pm0.0005^{\circ}$ 

Pin fit in gauge shall be such that gauge together with supplementary weight totaling 3 lbs. will not be lifted when pins are withdrawn.

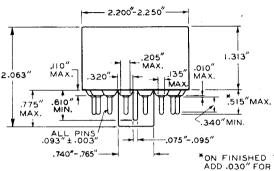
SMALL SHELL DUODECAL 7-PIN
As above, Omitting Pins No. 3,4,5,8 & 9
- No. 7253 -

MEDIUM SHELL DIHEPTAL 12-PIN
For details of this base, see corresponding
DIHEPTAL 14-PIN type

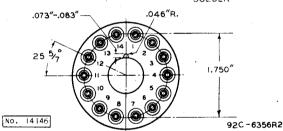
\* on finished tube, add .030\* for solder.



### MEDIUM SHELL DIHEPTAL 14-PIN



\*ON FINISHED TUBE, SOL DER



Base-pin positions are held to tolerances such that pins will fit flat-plate gauge having thickness of 0.25" and fourteen 0.1030"± 0.0005" holes so located on a 1.7500"± 0.0005" diameter circle that the distance along the chord between any two adjacent hole centers is 0.3900" ± 0.0005".

Pin fit in gauge shall be such that gauge together with supplementary weight totaling 3 lbs. will not be lifted when pins are withdrawn.

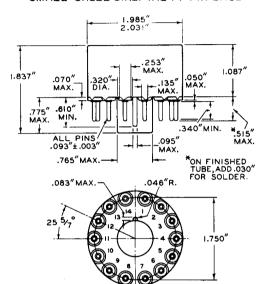
> MEDIUM SHELL DIHEPTAL 12-PIN As above, Omitting Pins No. 6 & 13 -No. 12146-

APRIL 1. 1946





# SMALL-SHELL DIHEPTAL 14-PIN BASE



# BOTTOM VIEW OF BASE

No. 14151

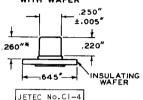
92CM - 6580

Gauge information is the same as that shown for MEDIUM-SHELL DIHEPTAL 14-PIN BASE

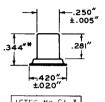


1 - TERMINAL TYPES (CAPS)

# MINIATURE WITH WAFFR



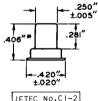
# SKIRTED MINIATURE



JETEC No.CI-3 RCA No.3933

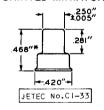
# SKIRTED MINIATURE

RCA No.M-399



JETEC No.CI-2 RCA No.3927

# SKIRTED MINIATURE

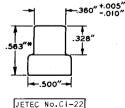


# SMALL .360" ±.005" 406"\* <del>-.</del>420″→ ±.020"

JETEC No.CI-I RCA No.3907

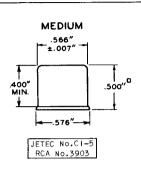
Add 0.020\* for solder on finished tube.

### SKIRTED SMALL

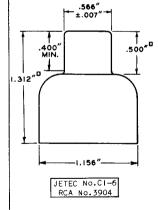




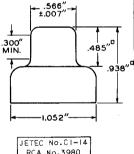
1 - TERMINAL TYPES (CAPS)



# SKIRTED MEDIUM



# SKIRTED MEDIUM

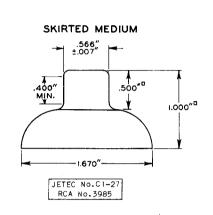


RCA No.3980

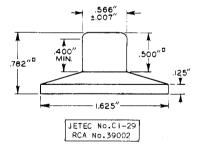
D Add 0.040\* for solder on finished tube.



# 1 TERMINAL TYPES (CAPS)



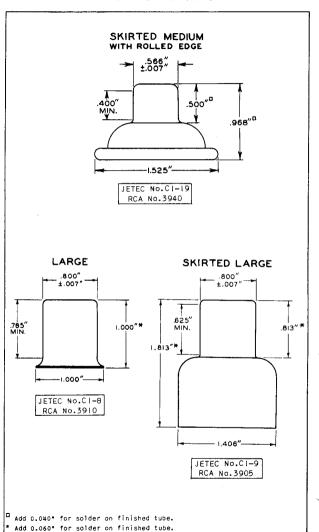
# SKIRTED MEDIUM



Add 0.040" for solder on finished tube.

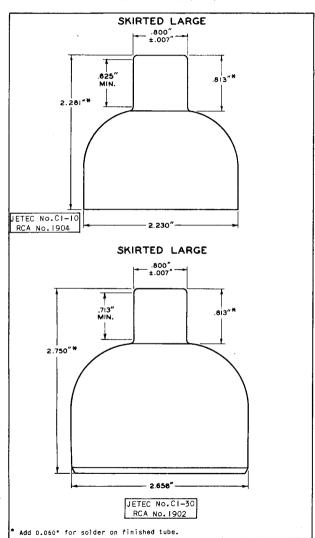


1 TERMINAL TYPES (CAPS)





## 1-TERMINAL TYPES (CAPS)

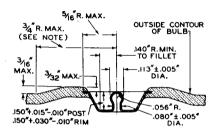




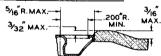
1-TERMINAL TYPES (CAPS)

# DETAILS OF RECESSED SMALL BALL CAP & BULB ASSEMBLY

JETEC No.JI-22



## ALTERNATE EDGE DESIGN



# VARIANT SEAL SHAPES



NOTE: PROTRUSION OF GLASS AROUND CAP ABOVE BULB CONTOUR IS LIMITED TO AREA BOUNDED BY CIRCLE CONCENTRIC WITH CAP AXIS AND HAVING RADIUS OF 3/4" MAX.

FOR ATTACHING OR DETACHING, THE CONNECTOR SHOULD REQUIRE NOT MORE THAN 8 POUNDS TOTAL FORCE PERPENDICULAR TO THE PLANE OF THE RIM OF THE CAP.

ANGLE BETWEEN PLANE OF THE RIM OF CAP AND PLANE TANGENT TO ORIGINAL CONTOUR OF BULB AT CENTER OF CAP WILL NOT BE MORE THAN 10°.

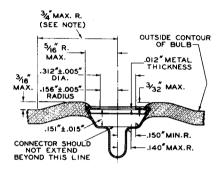
92CM-6535R4



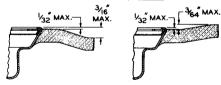
1-TERMINAL TYPES (CAPS)

# DETAILS OF RECESSED SMALL CAVITY CAP & BULB ASSEMBLY

JETEC No.JI-21



## VARIANT SEAL SHAPES



NOTE: PROTRUSION OF GLASS AROUND CAP ABOVE BULB CONTOUR IS LIMITED TO AREA BOUNDED BY CIRCLE CONCENTRIC WITH CAP AXIS AND HAVING RADIUS OF 3/4" MAX.

FOR ATTACHING OR DETACHING, THE CONNECTOR SHOULD REQUIRE NOT MORE THAN 8 POUNDS TOTAL FORCE PERPENDICULAR TO THE PLANE OF THE RIM OF THE CAP.

CONNECTOR SHOULD PROVIDE POSITIVE SPRING CONTACT TO TOP AND BOTTOM INTERIOR SURFACES. IT SHOULD NOT MAKE CONTACT TO THE INSIDE TOP SURFACE ONLY.

ANGLE BETWEEN PLANE OF THE RIM OF CAP AND PLANE TANGENT TO ORIGINAL CONTOUR OF BULB AT CENTER OF CAP WILL NOT BE MORE THAN 10°.

92CM-665IR2